

BAINBRIDGE TWP.

Taylor Road

83

LEVEL BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROAD TO SIDES FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE WITH SIDE SLOPES 1 TO 1
FOR SINGLE TRACK EXCAVATION.

PLEASE RETURN TO GEAUGA COUNTY ENGINEER COURT HOUSE

Copyright 1955, by Keuffel & Esser Co.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 0 |
| 1 | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 1 |
| 2 | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 2 |
| 3 | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 3 |
| 4 | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 4 |
| 5 | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 5 |
| 6 | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 6 |
| 7 | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 7 |
| 8 | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 8 |
| 9 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 9 |
| 10 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 10 |
| 11 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 11 |
| 12 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 12 |
| 13 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 13 |
| 14 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 14 |
| 15 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 15 |
| 16 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 16 |
| 17 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 17 |
| 18 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 18 |
| 19 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 19 |
| 20 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 20 |
| 21 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 21 |
| 22 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 22 |
| 23 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 23 |
| 24 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 24 |
| 25 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 25 |
| 26 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 26 |
| 27 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 27 |
| 28 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 28 |
| 29 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 29 |
| 30 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 30 |
| 31 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 31 |
| 32 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 32 |
| 33 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 33 |
| 34 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 34 |
| 35 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 35 |
| 36 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 36 |

Calculated by Julion A. Hall, M. Am. Soc. C. E.

BAINBRIDGE TWP.,

186 Taylor^{-May} Road, from Chillicothe Road
to Snyder's Cor. Road. Pg. 1.

186 Taylor-May Rd. fr. Snyder's Cor's Rd to
Brown's Cor's Rd (Munn Rd) Pg. 55

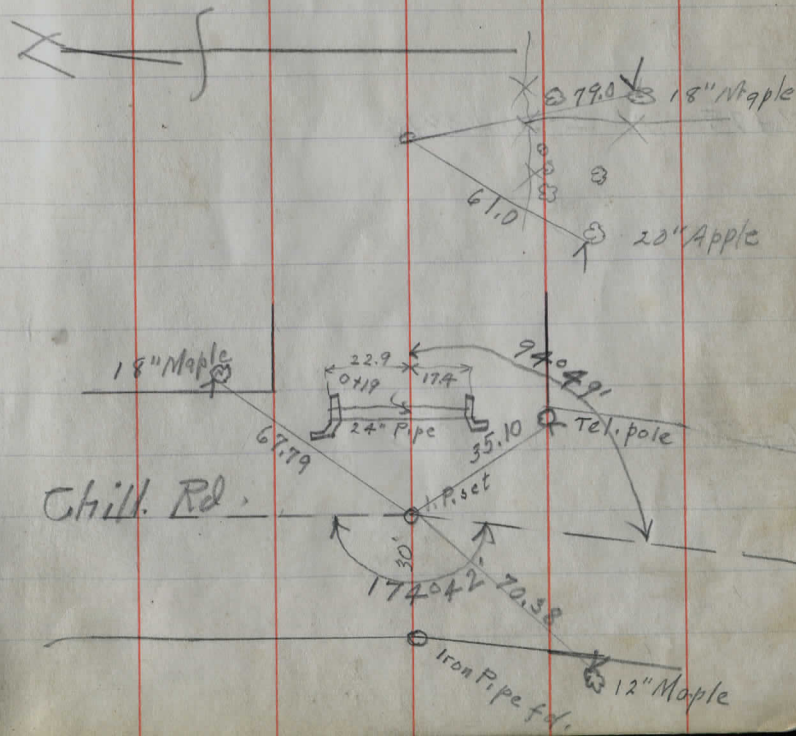
#186 Taylor-May Rd
(Munn Rd east to Auburn Rd) Pg. 62

83

1
Crew #83 C.S.R.

14+00 $\Delta = 0^\circ 42' L$

0+00 = P.I., Sta 79+51.47, Chillicothe Rd.

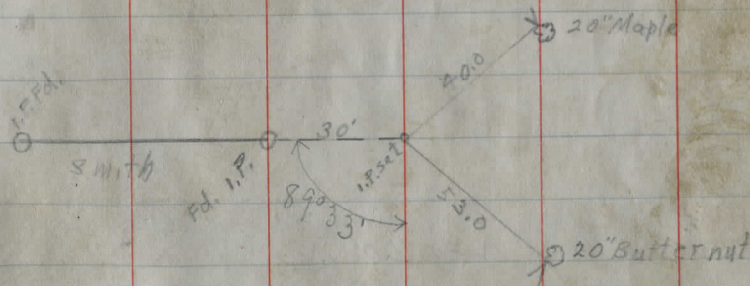
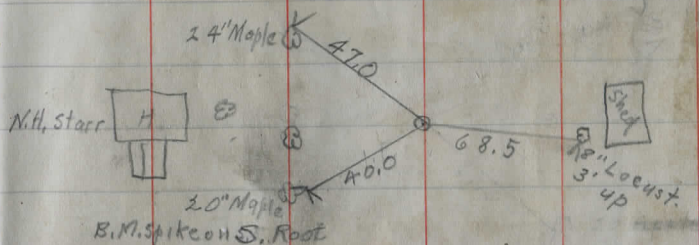
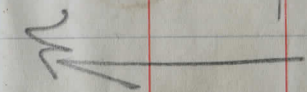
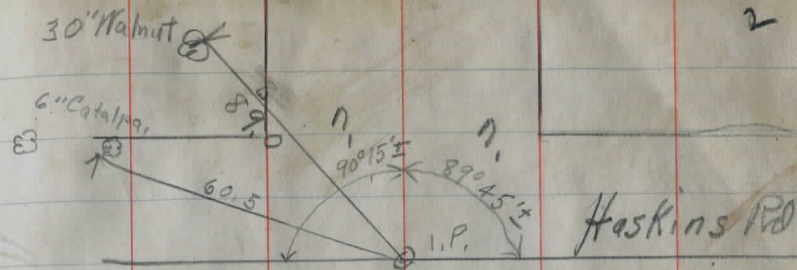


Stopped, Sept 27, 1929 Showers, 70°
 Marks, Parks, Goodrich

43+76.6 \neq N+S, Rd $\Delta = 0^{\circ}12\frac{1}{2}'L$.

28+75 $\Delta = 0^{\circ}42'R$

26+71.42 $\Delta = 0^{\circ}00'$

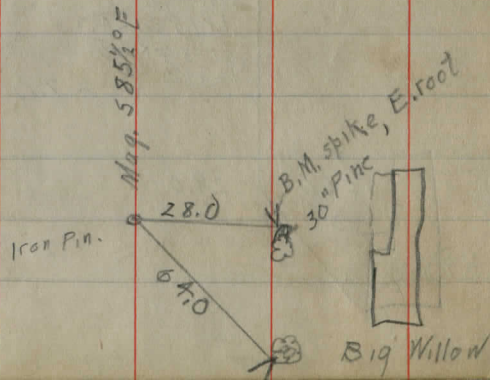
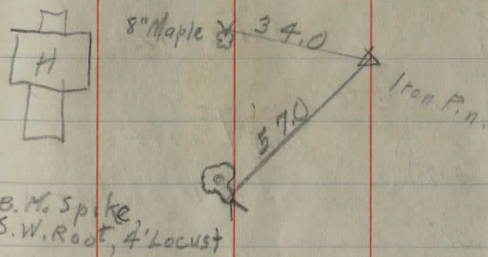
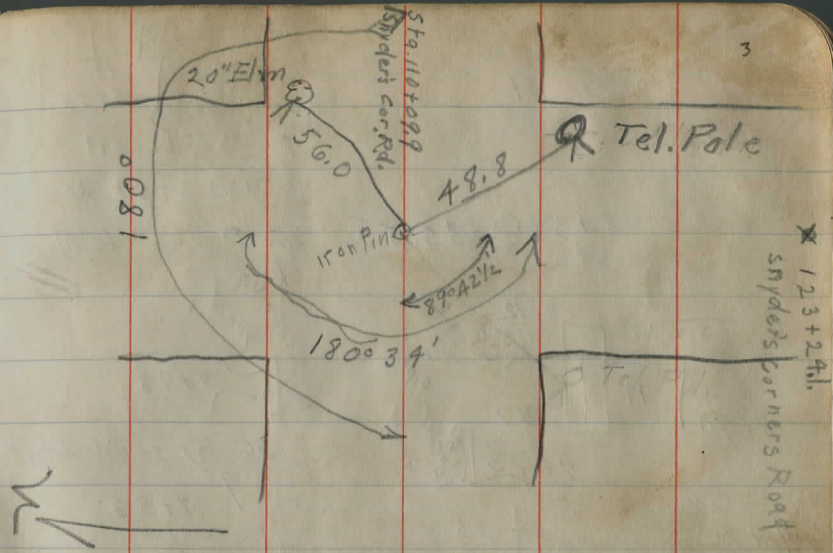


82+77.8. \pm , Snyder's Corners Road

75+00 $\Delta = 0^{\circ}00'$

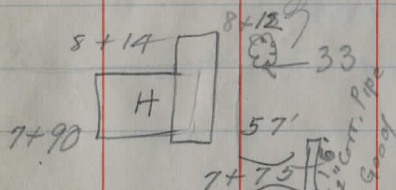
59+00

$\Delta = 0^{\circ}00'$



30" Maple 9+00 @ 31

8+39 @ 35.5
42" Locusts,

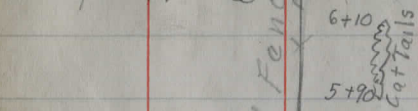


7+22 x x 25.5

8" Elm 7+01 @ 27'

42" Maple 6+52 @ 30'

20" Maple 5+95 @ 28



3+00 @ 30'

2+70 @

2+20 @

Saplings,

7+95 @ 24.5

1+03 @ 25

1+48 @ 20

0+40 @ 29.0
6" Elm

6+27.5

28.5 @ 80+ 8+55

29 @ 8" Locust 8+51

29.5 @ 8+34 20" Maple

32 @ 8+20 18" Maple

7+98

36 @ 24" Maple 9+88

23 T 7+83

24 T 6+12

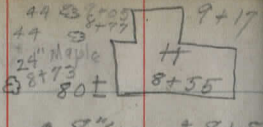
25.5 T 4+44

30.5 @ 18" Walnut 4+30

26 T 2+83

27.0 T 1+31

28.5 T 0+21.5



14+69 @ 25

10" cherries

14+47 @ 23

14+02-15" Maple @ 24.5

13+84 35" Chestnut @ 20.5

13+09 10" Walnut @ 26.5

12+98 12" Chestnut @ 26.5

12+81 6" Cherry @ 26

8" cherry 12+40 @ 25.5

18" Maple 11+89 @ 24.5

11+01 @ 27.5

15" Apple 10+74 @ 27.5

15" Locust

10+29 @ 27.5

9+31 @ 28'

Requires 15" Hillside Grave

14+93

13.8

27.0 @ 14+65

14+21

18" Maples @

14+15.5

18.5 T 14+07

26.0 @ 6" Butternut 12+98

25.0 @ 12" Elm 13+95

24.5 @ 18" Maple 13+82

26.5 @ 15" W. Cherry 13+41

21 @ 13+25 8" Maple

19.5 T 12+84

22.5 @ 11+95

23 @ 11+73

27.5 @ 8" Elm 11+48

25.5 @ 12" Maple 11+45

25 @ 10" Cherry 11+30

20.5 T 11+23

25.5 @ 12" Maple 11+21

25.5 @ 8" Maple 11+05

23.0 @ 10" Maple 10+89

22.5 @ 12" Elm 10+61

21.5 T 9+76

45.5 @ Apples

25 @ 9+75

0

Orchard

18.5 T 22+80

21+83 8" Corr. Pipe
Fall
Requires 15" 6.9 9.5 →

20" Maple 21+43

21+00 18.0 T 21+03
22.5 X

8" Trees

20+90

22.5 10" Cherry 19+79

21.5 10" Walnut 19+33

18.5 T 19+31

19+00 X

8" Trees

18+35

27 24" Maple 18+21

26 15" Maple 17+81

23 8" Elm 17+64

17+62 12" Corr. Pipe
good
Requires 15" 3.0 13.2 →

17+00

16+97 8" Maple 24.5

16+66 20" Maple 5

15+86 8" Cherry 24.5

15+34 24" Maple 25

15+13 12" Walnut 24

19 T 17+53

22.5 15" Walnut 17+45

23.0 X 17+36 P.L.?

27.0 16+90 20" Maple

21.5 X 12" Walnut 16+73

28.5 10+14

22.0 16+15+83

18.5 T 15+76

26.5 15+53

28.5 15+15

19.5 T 30+30

17 X 30+25

8" Iron Pipe
Battered 30+10

30+22 (5)

29+65 X

29+20

29+11 24" Maple 30

28+97 4. Hemlock
400' Maple
28+18 30.5

28+65

28+47 20" 30.5

27 30" Walnut 28+99

28+91

25.5 T 28+75 70' Shed

28+67

27 18" Maple 28+79

27 28+29 28" Maple

28+26

19.0 X 28+12 70'

22.1 X

27+95

23.5 20" Locust 27+64

26.5 15" Maple 27+15

26 27' or 18" Maple

Start 26+82 8" Maple 28

26+71.4 30'

Smith 26+08 32.0

25+64

25+35 10" W. Cherry 25.5

27 24" Locust 26+71

18.5 T 26+40

29 24" Walnut 26+76

30 24" Maple 25+68

25+14 15" 18' or 12' P.L.?

29 24+91

23 24+91

18.5 T 24+63

24+36 24" Maple 26.5

23 30" Walnut 24+28

23+50 P.L.?

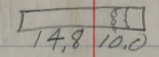
24 24" Maple 23+38

Milk House 29+21

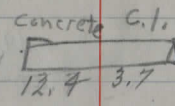
Shed

RAVINE

Pipe good to use again 20' sec. l. 4" Vit. Pipe
 37+82 15" Pipe, Requires 24" Pipe



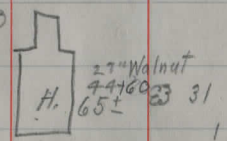
37+16 T 26.5
 35+67 T 26.5
 35+00 8" W. Cherry 17'
 34+15 12" Butternuts 31
 34+03 30.5
 33+80 T 26.5
 33+83 X X X 30
 33+33.5 12" Conc. Pipe Requires 15"
 33+00 Saplings
 32+80
 32+27 T 26.5 Saplings 31+90
 31+16 15" Maple 28
 30+76 T 26.5
 30+58 29.5
 30+50 29.0
 30+31 18" W. Cherry 29



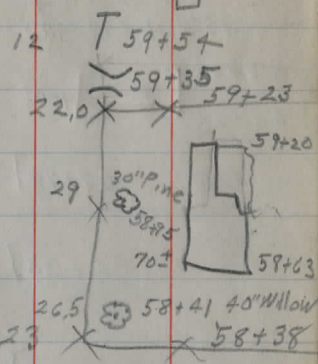
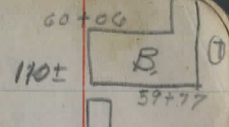
47+02 T 22.5
 47+00
 45+48 T 23.5
 45+10
 44+54 H. 27" Walnut 44+60 33 31 65±
 43+99 T 26.5
 43+76.6
 43+57 IIII 38
 42+56 T 26.5
 41+31 T 26.5
 41+20 16" 15' sec. l. pipe Gas
 39+86 T 27
 38+59 T 27
 15 58" cherry 47+73
 15 clump, 8" Elms 47+69
 17.5 T 47+67
 22 15" Elms scrub 46+35
 23 12" W. Cherry 46+14
 22.5 8" Elm 46+08
 21 10" Scrub Cherry 45+96
 19.5 45+85
 21 10" W. Cherry 45+62
 19.5 T 43+99
 35 X X 43+54
 22 X 42+85
 20.5 X 42+41
 21 T 40+63
 21.5 T 38+89
 22.5 X X 38+47 P.L.
 38+31

Cat tails.

Brush + Saplings.



Pole Pipe from Millicut head



OSAGE Hedge

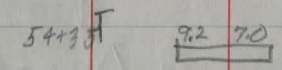
57+31 T 37
57+00 24.5

13 T 57+83

T 56+14

55+86 T 22.5

54+19
8" Corr Pipe Fair
requires 15"



54+38 T
52+66 T

T 54+43
Old Corner Post
20.5 P.L.
53+29

51+38 T 22

T 52+70

49+90 T 22.5

16.5 T 51+03

49+70
cat tails

16.5 T 49+34

48+45 T 22

19.5 8" Cherry 48+66

15 8" Elm 48+20

70±02 27'
12" Maple
69+72

17.0
78+06
78+06

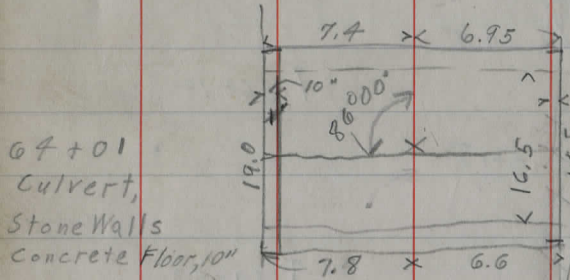
69+16 T
15" Maple 69+04 26.5

68+43
68+20 [B] 100±

67+78 T

66+33 T 22

64+95 ← 24



63+33 T 32

62+67
62+60 28
62+09

Osage Hedge

12 T 62+94

23 61+80 20" Apples
24 61+62
16 61+34
20

13 T 61+25

T 69+77

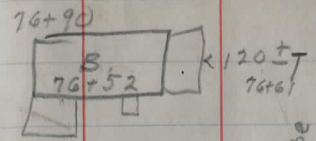
68+40

T 68+02

11.5 T 66+37
16 15" Apple
65+09

10 T 64+72

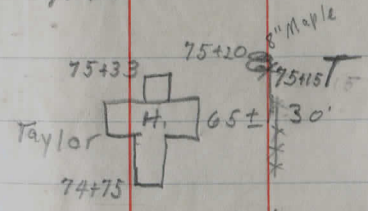
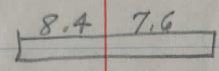
79+57 T
78+10 T



76+35 16" Sec. C.I. Pipe

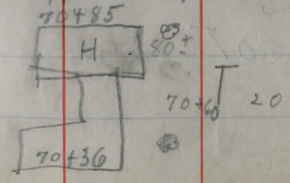
18" Hickory
76+04 31

75+44
10" Sec. C.I. Pipe
req. 15"



74+75
74+56 74+63 48" Locust 34.5
74+48 30" Apple 36.5

73+60 T
72+11 T
20" Apple 71+21 33'

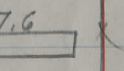


T 79+57

T 77+84

16.5 T 76+47

76+33



16 T 74+80

16.5 74+54 8" Pine

T 73+25

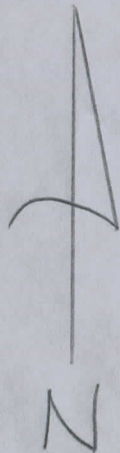
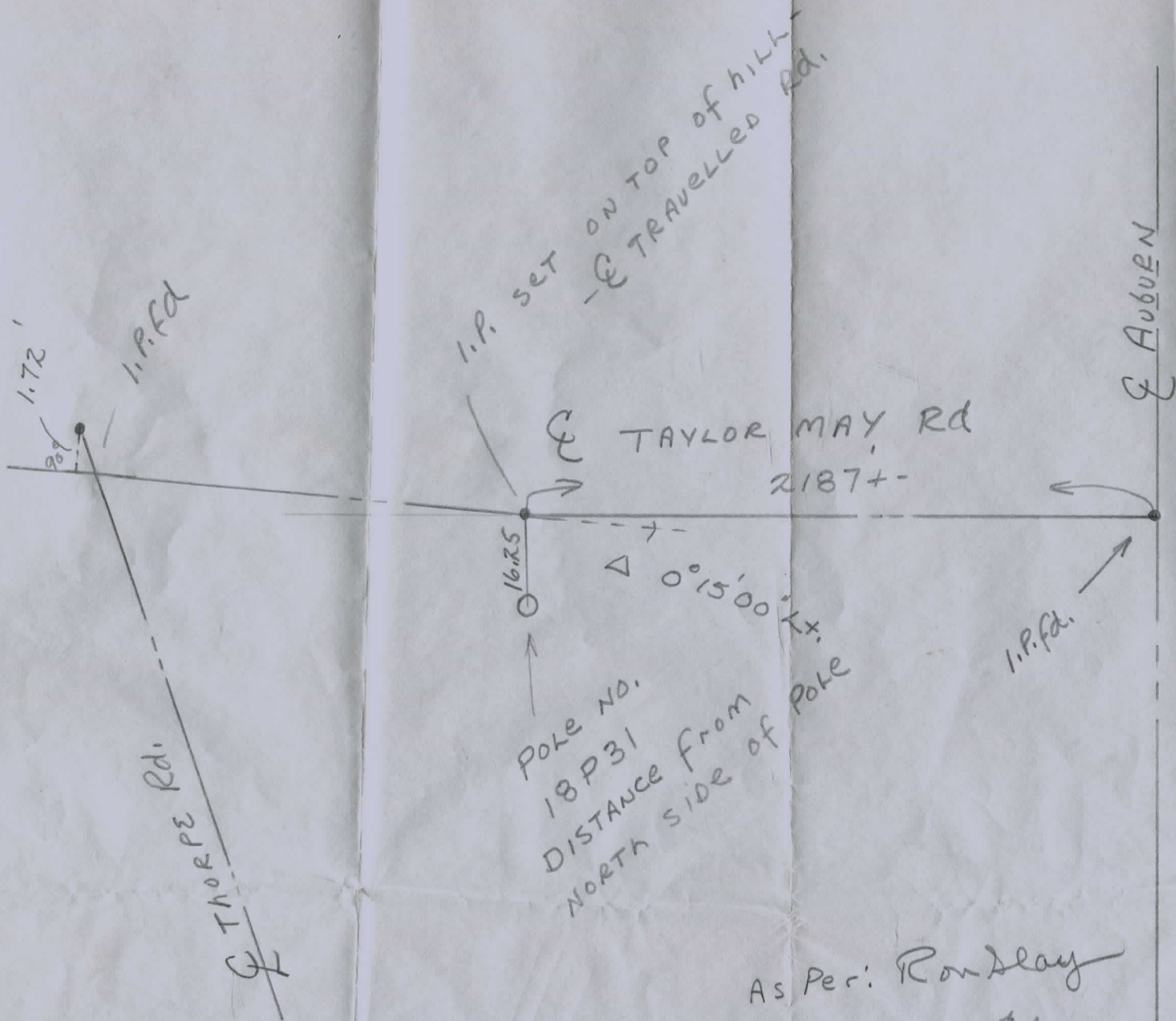
T 71+49

Finished Topography, 3:10 P.M. Oct. 1, 1929
Cloudy, 55° Marks, Parks, Goodrich

81+84 T 23.0

18.0 T 81+30

80+70 T 22.5



As Per: Ron Slay

Jerry SLAY & Assoc.
129 MAIN ST.
CHARDON, OHIO

15.79 1070.32 ✓ 1054.53 ✓

16.04 1082.05 ✓ 4.31 1066.01 ✓

7.00 1075.05 ✓

0+00 7.2 1074.9

0+30 6.0 1076.1

1+00 2.9 1079.2

I.P. 14.79 1096.50 ✓ 0.34 1081.71 ✓

2 14.8 1081.70

3 12.1 1084.4

4 8.6 1087.90

14.81 1107.28 ✓ 4.03 1092.47 ✓

5 14.8 1092.5

6 8.0 1099.3

15.65 1120.84 2.09 1105.19

Spoke in SE root, 30" Elm, 35' Left Sta. 67+00

B.M. #7 (New) Chillicothe Road

N.E. Cor, F.H.W., Culvert, Sta 75+00 Chillicothe Rd.

across Taylor Rd.

X on S.E. cor, S.H.W. Culvert, on E. side Chillicothe Rd.

1078.3 1077.4 1076.9 1075.6 1073.3
3.8 4.9 5.7 6.5 6.8 7.2 7.6 8.0 8.7 9.1 10.8
270 250 200 30.1 30.0 30.0 30.0 50.0 100.0 150.0 200

3.9 5.5 7.4 9.9 5.7 6.0 7.5 10.4 6.6 6.6
36.5 27.5 26.0 21.5 11.5 9 13.5 20.0 24.5 30.0

3.2 3.6 3.6 4.7 9.1 2.9 2.9 3.0 3.2 3.3 4.1 4.4 3.4
30. 27 16. 14. 11.5 9 2.0 35 5.0 9.0 11.0 130-15.0 16.3

15.8 16.4 16.9 15.0 14.8 14.9 15.8 14.8 14.8 15.8
30. 10.5 9.0 7. 9 7 10.5 14.0 20.5 30

12 11.8 12.2 12.5 12.0 12.1 12.0 12.2 13.4 12.6 11.2 10.1
30 25 14 13 11 9 4 6.5 8 9 13.5 30

5.5 6.0 10.8 8.8 8.6 8.6 9.6 7.4 7.0 7.7
30 13.5 5.5 4 9 11.5 14 19 25 30

10.4 10.4 11.2 13.0 15.9 14.8 14.8 14.5 14.2 13.0 11.9 12.0
30 - 25 14.5 10 9 8 9 12.5 15.5 17 12.5 30

2.8 3.7 8.5 9.0 8.0 8.0 8.3 10.1 5.4 5.0 5.4
30 17 9.5 5 2 9 14 12.5 22 27 30

1120.84

7 15.7 1105.1

7+50 12.5 1108.3

8 8.5 1112.3

B.M. 5.34 1115.50

11.74 1132.33 0.25 1120.59

8+50 15.3 1117.0

9 11.5 1120.8

13.45 1142.57 3.21 1129.12

10 12.2 1130.4

11 6.9 1135.7

14.66 1155.46 1.77 1140.80

12 14.7 1140.8

13 10.1 1145.4

13.7
 11.1 12.1 15.9 15.6 16.7 15.7 14.1 16.5 15.6 13.6 12.7 13
 30 18.0 11.5 7.5 6.4 4 16 12.5 19-23 25 19 33

8.7 10.2 12.4 13.8 12.5 12.5 13.0 13.9 13.5 11.4 11.5
 30 13 2.5 4 3 4 15 19 22.5 27.5 35

2.0 6.1 7.3 9.7 8.5 8.5 9.2 10.0 9.2 9.7
 30 17.5 7 3.5 1.5 4 18 19 20 35

Spike in

N.W. root 20" Maple -30 17.5 to 8+30

5.3 6.3 7.7 9.3 15.5 17.5 15.3 15.3 15.4 17.6 15.4 14.8
 4.0 30 22.5 17.5 5.5 3.5 1 4 14 18 24 30

0.2 1.9 3.6 12.2 11.5 11.5 12.0 13.5 8.9 9.7
 4.0 25 18.5 4.5 3 4 14 16-18 22.5 30

6.0 6.3 7.1 12.0 11.6 12.2 12.5 13.0 12.5 10.9 11.0 13.1
 30 25 20.5 6.5 4.5 3.5 4 11 14 17 20 23.5 30
 rock rock

2.1 3.2 3.7 4.8 6.5 7.5 6.9 6.9 7.5 8.5 7.3 5.1 5.0
 30 25 19.5 15 11 6 2 4 10.5 7.3 16.5 18.5 30

9.3 9.1 10.1 10.7 14.8 15.8 14.7 14.7 14.5 15.0 16.2 14.9 12.9 13.9
 40 35 25 19 8 6.5 3 4 7.5 10.5 10 17 20 30
 rock rock

6.7 7.6 8.7 9.8 10.1 15.7 10.2 10.0 10.5 11.4 8.9 8.2 8.2
 35 25 18 13.5 7 5.5 4 5 9.5 12.5 18 23 30

rock

1155.46

14 6.0 1149.5

10.54 1162.04 3.96 1151.50

14+93 10.7 1151.3

15 10.6 1151.4

16 8.5 1153.5

B.M. 9.88 1166.43 5.49 1156.55

-16+50 10.7 1155.7

17 8.9 1157.5

17+62.1 7.9 1158.5

17+62.1 For Earth Work Calculations

18 7.6 1158.8

2.9 2.3 2.2 3.2 5.9 6.4 6.0 6.0 4.2 6.6 4.6 4.8
40 30 25 18 7.5 5 2 2 10 11.5 12.5 17 30

ROCK

2 Spike at Sta. 10+10

11.5 10.7 11.8 12.4 16.5
30 2 13.5 30 100

6.5 6.3 7.3 8.8 9.6 11.3 10.6 10.3 10.7 11.3 16.3 10.8 11.4
35 30 25 14.5 6 4 2 5 11 12.5 16 22 30

ROCK

3.9 3.3 4.2 4.6 6.0 8.5 7.7 7.7 8.0 8.8 6.4
30 19 17 8.5 5 2 6 12 15-16 17 -30

Bent Spike N.W. root 24" Maple 28.5' Pt. Sta. 16+14

5.4 5.2 6.1 6.7 8.2 11.0 10.7 10.6 16.0 11.6 8.4 8.8
30 25 19 7.5 4 1 2 5 11.5 14 17 30

4.7 5.8 6.8 8.9 8.9 8.5 8.3 8.5 9.2 7.7 7.9
30 5 2 1 2.5 6 13 16 22 30

7.0 8.1 8.3 8.3 7.9 7.7 8.9 9.4 9.9 12.2 13.6
30 6 30 4 6 13.2 30 50 75

8.4 9.0 9.5
17 27 30

5.6 7.1 7.9 8.7 7.6 7.3 7.8 8.6 7.9 7.1 7.4
30 7 5 3.5 4 7.5 12 15 16 23 30

1166.43

1171.05

11.26

~~1170.05~~

6.64

1159.79

19

11.3

1159.8

$$\frac{8.6}{30} \quad \frac{8.9}{12} \quad \frac{9.6}{5} \quad \frac{12.1}{3} \quad \frac{13.1}{2.7} \quad \frac{11.4}{11} \quad \frac{11.9}{13} \quad \frac{10.8}{15} \quad \frac{10.5}{20} \quad \frac{11.2}{30}$$

20

9.2

1161.9

$$\frac{6.1}{30} \quad \frac{6.5}{12.5} \quad \frac{7.6}{6.5} \quad \frac{10.0}{7.5} \quad \frac{9.2}{4} \quad \frac{9.0}{8} \quad \frac{9.3}{10.5} \quad \frac{10}{13.5} \quad \frac{8.8}{14} \quad \frac{8.0}{17} \quad \frac{8.8}{25} \quad \frac{8.8}{30}$$

20+50

8.1

1163.0

$$\frac{5.3}{30} \quad \frac{6.0}{10} \quad \frac{6.7}{6.5} \quad \frac{9.0}{5} \quad \frac{8.1}{2} \quad \frac{8.1}{4} \quad \frac{7.9}{3.5} \quad \frac{8.3}{9.5} \quad \frac{8.9}{12.5} \quad \frac{7.2}{14} \quad \frac{6.7}{20} \quad \frac{6.1}{27} \quad \frac{7.2}{30}$$

21

9.5

1161.6

$$\frac{4.6}{30} \quad \frac{5.5}{16.5} \quad \frac{6.7}{9.5} \quad \frac{10.4}{5.5} \quad \frac{9.5}{3} \quad \frac{7.5}{4} \quad \frac{9.4}{9.5} \quad \frac{9.8}{9} \quad \frac{10.7}{12} \quad \frac{9.6}{12.5} \quad \frac{7.4}{14} \quad \frac{7.2}{17} \quad \frac{7.8}{25} \quad \frac{7.8}{30}$$

21+50

10.9

1160.2

$$\frac{6.6}{30} \quad \frac{8.0}{18.5} \quad \frac{10.5}{11.5} \quad \frac{11.1}{8.5} \quad \frac{10.8}{6.5} \quad \frac{10.9}{4.5} \quad \frac{10.9}{4} \quad \frac{11.1}{7.5} \quad \frac{12.0}{10} \quad \frac{11.7}{11.5} \quad \frac{14.4}{30}$$

21+83

10.6

1160.5

$$\frac{12.0}{30} \quad \frac{13.3}{6.7} \quad \frac{11.2}{5.5} \quad \frac{10.7}{3.5} \quad \frac{10.6}{4} \quad \frac{11.2}{8.5} \quad \frac{13.7}{9.5} \quad \frac{14.2}{30} \quad \frac{16.9}{50} \quad \frac{23.0}{100}$$

22

10.5

1160.6

$$\frac{10.7}{30} \quad \frac{11.0}{9} \quad \frac{12.1}{9} \quad \frac{10.6}{4.5} \quad \frac{10.5}{4} \quad \frac{11.8}{8} \quad \frac{11.6}{9.5} \quad \frac{11.2}{11} \quad \frac{13.1}{25} \quad \frac{14.1}{30}$$

23

8.9

1162.2

$$\frac{1.5}{30} \quad \frac{2.5}{30} \quad \frac{3.9}{18} \quad \frac{10.0}{9.5} \quad \frac{9.0}{5} \quad \frac{8.9}{4} \quad \frac{10.1}{9} \quad \frac{6.0}{17} \quad \frac{6.0}{25} \quad \frac{6.8}{30}$$

24

4.3

1166.8

$$\frac{7.04}{30} \quad \frac{0.8}{13} \quad \frac{5.8}{7} \quad \frac{4.5}{3.5} \quad \frac{7.3}{4} \quad \frac{7.2}{3} \quad \frac{4.6}{8.5} \quad \frac{5.5}{11} \quad \frac{2.2}{14} \quad \frac{3.3}{30}$$

1176.75

7.02

~~1175.75~~

1.32

1169.73

~~1168.73~~

~~1176.75~~
~~1175.75~~

25 7.0 1169.8

26 5.9 1170.9

8.06 ~~1183.28~~ 0.53 ~~1175.22~~
1184.28 1176.22

27 11.0 1173.3

28 6.9 1177.4

B.M. 1.23 ~~1182.05~~
1183.05

7.0 4.7 7.4 8.6 7.0 7.0 7.4 8.0 7.3 8.5 9.6 9.9
~~30 18 8-6 5. 2 4 11.5 13.5 15 18.5 25 30~~

Right

Left

~~4.1 5.8 4.5 5.6 5.2 5.9 6.7 5.9 4.7 3.5 4.0~~
~~30-25 16.5 15.5 12.5 6 4 2 3 12 25 30~~

9.8 6.8 11.0 11.3 11.0 10.5 10.4 10.8 11.5 9.7 9.5
~~30 12 3 1.5 4 1.5 6.5 12 14 16.5 21-30~~

2.5 3.0 4.7 5.1 7.3 6.7 6.6 7.0 7.2 5.9 6.2
~~35 27 17 35 2 4 6.5 12 13.5 16 25-30~~

South Root 20" Maple 30' Left, 28 + 47

Stopped, Oct. 4, 1929, Cloudy, 50°

Marks, Parks, Goodrick

B.M. 0.73 ~~1182.78~~ 1183.78 ~~1182.05~~ 1183.05

28+75 4.3 1179.5

29 4.7 1179.1

29+50 5.8 1178.0

30 8.0 1175.8

30+50 11.0 1172.8

31 11.7 1172.1
1175.00 1171.99
3.01 ~~1174.00~~ 11.79 ~~1170.99~~

32 4.2 1170.80

33 5.8 1169.2

33+33.5 6.1 1168.9
Culvert Design only

South root 20" Maple 30' Left str. 28147

0.8 2.6 3.4 4.3 4.3 4.2 4.8 4.5 5.5
30 6 25 2 4 3 16 20 30

1.2 2.9 3.2 4.8 4.7 5.0 5.4 4.8 6.2
30 8 35 3 4 11 14.5 17 30

1.9 4.0 6.3 5.9 5.8 5.7 6.2 6.8 5.4 6.7
30 6.5 5 2 4 4 9 13 14.5 30

3.5 4.3 7.2 8.3 7.9 8.0 8.2 8.9 7.9 8.3
30 17 8.5 7 4.5 4 5 10 11 30

8.3 9.8 11.1 11.5 11.1 11.0 11.3 11.7 11.0 10.4 10.7
30 15 10 9 5 4 6 9 10 22 30

11.2 11.2 12.0 13.0 12.1 11.7 12.1 13.1 12.9 12.7 14.4
30 25 12 9.5 6 4 6 9 10.5 15 30

2.2 2.7 5.0 5.4 4.6 4.2 4.4 5.4 4.3 4.5 5.4 5.7
30 20 12 25 7 4 4.5 8 12 15 21 30

3.3 3.5 4.1 6.2 6.6 5.7 5.5 5.8 6.2 6.6 6.4 6.6 7.7 8.4
30 23 16 14 12 25 3 4 4 5.5 7 12 18 30

6.8 8.9 6.1 8.2 9.5 12.2
30 12.4 4 3.7 30 50
FL FL

1175.00
~~1174.00~~

1179.84

1169.33

T.P 10.51

~~1175.84~~ 5.67~~1168.35~~

33+50

10.9

1168.9

34

10.5

1169.3

34+50

9.8

1170.0

35

11.6

1168.2

1175.36

1168.24

7.12

~~1174.36~~ 11.60~~1167.24~~

35+50

9.1

1166.3

36

12.5

1162.9

36+50

16.2

1159.2

1164.08

1159.90

4.38

~~1163.08~~ 15.66~~1158.40~~

37

6.2

1157.9

37+82

7.9

1156.2

4 spike at sta. 34

| | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|------|------|
| 11.2 | 11.5 | 11.4 | 11.8 | 10.7 | 10.9 | 11.1 | 11.6 | 11.9 | 12.8 | 13.7 | 14.0 |
| 30 | 22 | 18 | 11.5 | 8 | 7 | 3.5 | 5.5 | 8 | 13 | 21 | 30 |

| | | | | | | | | | | | |
|-----|-----|-----|------|------|------|------|------|------|------|------|------|
| 4.5 | 6.0 | 8.4 | 10.6 | 11.2 | 10.7 | 10.5 | 10.6 | 11.6 | 10.8 | 11.4 | 11.6 |
| 35 | 27 | 21 | 12 | 10 | 8 | 7 | 3.5 | 7.5 | 15 | 21 | 30 |

| | | | | | | | | | | | | | |
|-----|------|------|------|------|------|-----|------|------|------|------|------|------|------|
| 5.5 | 6.2 | 8.7 | 9.7 | 10.5 | 10.1 | 9.8 | 10.1 | 11.1 | 10.2 | 10.5 | 11.0 | 11.3 | 11.8 |
| 33 | 23.5 | 16.5 | 11.5 | 9 | 6 | 7 | 4.5 | 8 | 9.5 | 15 | 20 | 24 | 30 |

| | | | | | | | | | | | |
|-----|-----|------|------|------|------|------|------|------|------|------|------|
| 6.7 | 7.9 | 11.3 | 12.4 | 12.2 | 11.6 | 11.8 | 12.4 | 11.5 | 10.8 | 11.7 | 11.9 |
| 35 | 19 | 11 | 8.5 | 7 | 7 | 5 | 8.5 | 9.5 | 12 | 20 | 30 |

4 spike at sta 35

| | | | | | | | | | | | |
|-----|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|
| 3.7 | 5.0 | 7.5 | 9.9 | 9.5 | 9.1 | 9.4 | 10.3 | 8.4 | 7.7 | 8.4 | 9.4 |
| 35 | 28.5 | 13 | 8.5 | 6.5 | 7 | 5 | 8.5 | 9 | 13 | 20 | 30 |

| | | | | | | | | | | | | |
|-----|-----|------|------|------|------|------|------|------|------|-----|------|-----|
| 5.5 | 5.3 | 6.7 | 12.5 | 13.7 | 12.7 | 12.5 | 12.7 | 13.6 | 12.1 | 9.0 | 9.2 | 9.2 |
| 35 | 30 | 19.5 | 10 | 9 | 6.5 | 7 | 4 | 7.5 | 8 | 14 | 21.5 | 30 |

| | | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 11.3 | 12.3 | 13.9 | 16.1 | 17.1 | 16.2 | 16.2 | 16.5 | 17.4 | 16.7 | 14.6 | 14.4 | 15.0 |
| 35 | 20.5 | 13.5 | 11.5 | 10 | 9 | 7 | 4.5 | 7 | 7.5 | 13 | 21 | 30 |

| | | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| 5.4 | 6.1 | 6.7 | 7.3 | 6.7 | 6.2 | 6.4 | 7.1 | 7.0 | 7.3 | 8.6 | 10.6 |
| 30 | 12 | 11 | 7.5 | 8 | 7 | 4.5 | 7 | 8.5 | 12 | 20 | 30 |

1153.2

1151.9, 1152.3

| | | | | | | | | | | | | |
|-----|-----|------|------|-----|-----|-----|-----|------|------|------|------|------|
| 7.1 | 9.1 | 10.9 | 8.0 | 7.5 | 7.9 | 8.1 | 9.3 | 12.2 | 11.9 | 12.0 | 12.2 | 12.8 |
| 50 | 25 | 15.8 | 14.5 | 8 | 7 | 5 | 8.5 | 10 | 19 | 30 | 50 | 100 |

| | |
|------|------|
| 13.5 | 14.8 |
| 150 | 200 |

1164.08
~~1163.08~~

38 8.1 1156.0

39 7.3 1156.8

9.41 1166.18
1165.18 7.31 ~~1155.77~~

40 7.8 1158.4

41 5.5 1160.7

8.56 1171.23
1170.23 3.51 ~~1161.67~~

42 8.6 1162.6

43 6.5 1164.7

43+76.6 \$ N, & E, 100 4 5.5 1165.7

44 5.1 1166.1

44+50 5.4 1165.8
1169.64

B M 1.59 ~~1168.64~~

45 7.1 1164.1

8.4 8.8 8.2 9.7 9.5 7.8 8.1 8.2 9.1 8.6 9.4
30 18 13 11 9 8 4 4.5 6.5 7.5 20-30

6.9 7.6 8.2 7.4 7.3 7.5 8.1 7.8 7.5 6.2 6.0
30 12.5 11-9.5 8 4 5 6-8 8.5 11.5 16 30

4 spike at sta. 39

4.7 6.1 6.7 7.8 7.7 9.3 8.2 7.8 8.1 8.1 5.9 5.6 5.8
30-25 20.5 17 15 12.5 10.5 7 4 4.5 7.6 7.5 25 30

4.9 5.0 5.5 7.0 6.0 5.5 5.9 6.8 5.9 4.6 7.0 4.3
30-25 20 15.5 11-9 7.5 4 4.5 8 10.5-12.5 15 24 30

2 spike sta 42

8.2 8.7 9.9 7.9 8.6 8.9 9.8 9.0 7.7 6.8 7.2
30 13 9.5 6 4 6 9 11 14 24 30

5.2 5.7 6.3 7.6 6.8 6.5 6.7 7.7 6.7 5.8 5.4 5.9
30 25 11 9 4.5 4 7 11.5 13-15 18 24 26.5 30

0.6 2.1 3.6 4.7 5.5 6.6 6.8 7.4 8.0 8.7 9.1 9.7 11.3 13.7
150 100 50 15.5 4 80 50 100 150 200 250 300 350 400
1170.6 1169.1 1167.6 1166.5 1164.6 1164.4 1163.8 1163.2 1162.5 1162.1 1161.5 1159.9 1157.5

4.5 5.1 7.3 5.0 5.1 5.3 5.9 5.6 5.6
30-20 18 7.5 10 4 8 14 23 30

R.P. spike S.E. side trunk 27 "Walnut 31 Lt. 4476

3.3 3.5 4.1 6.3 8.4 7.8 7.1 7.0 7.4 7.7 6.2 5.1
30 25 19 11 7.5 6 4 2 7.5 9-11 12.5 16-19

4.6 5.5
23.5 30

1171.23
~~1170.23~~

45+50 11.1 1160.1

46 14.5 1156.7
1158.03
~~1157.43~~ 14.53 1155.70
1.33

46+50 3.5 1154.5

47 7.5 1150.5

47+50 11.9 1146.1

48 14.3 1143.7
1146.22
~~1145.22~~ 14.24 1142.79
2.13

49 6.0 1140.2

50 8.8 1137.4

51 10.9 1135.3
1136.49
~~1135.49~~ 10.86 1134.86
1.13

52 3.0 1133.5

5.4 5.4 5.3 11.0 12.4 11.5 11.1 11.4 12.2 5.7 7.2 6.6
35 30 19.5 9 75.6 4 7 11.1 21.5 30 35

10.5 10.8 15.2 17.9 14.5 15.0 16.0 11.0 11.5
~~35 25 15.5 9 6.5 4 9 12 21 30~~

4 spike sta 46

2.3 2.5 3.6 3.7 4.5 3.7 3.5 3.7 4.8 3.8 3.1 3.5
30 17 135 11 9 6.5 4 8.5 11.5 12.5 20 30

5.3 5.3 6.9 8.4 7.1 7.7 7.5 7.6 8.6 6.7 4.3 4.9
30 25 13 14.5 7 6.5 4 9 10.5 12.5 18 30

8.0 9.3 11.3 13 12.5 11.9 12.1 12.9 11.4 9.4 9.1 10
35-25 15 9.5 7 6-3.5 4 7.5 9 11.5 16.5 24 30

10.8 11.3 12.3 14.0 14.1 15.7 14.7 14.3 14.6 15.7 14.1 12.0 12.1 12.9
30 20 14.5 11.5 9.5 7.5 6-3.5 4 8.5 10.5 12-14 17 25 30

4 spike sta 48

4.4 4.3 4.9 5.5 5.7 4.9 6.3 6.0 5.8 6.2 7.6 6.7 4.9 4.8 5.5
30 24 17 14.5 10.5 7.5 6 4 2 10 11.5 13 19 25 30

9.2 8.8 9.2 9.4 10.1 9.0 8.8 8.9 9.2 10.5 9.6 8.8 8.5 8.9 9.4
30 25 20 10 8.5 6 4 6.5 8.5 12 13.5 17 21 27.5 30

11.4 10.8 11.7 11.5 12.5 11.1 10.9 10.7 11.4 12.4 11.9 11.7 12.2 12.7 12.0
30 24 18 10.5 8.5 7 4 1.5 9 11.5 13 17 20 27 30

4 spike sta 51

3.4 3.3 3.8 3.5 4.3 3.4 3.0 3.4 4.6 3.9 3.8 4.4 5.2
30 25 20 9.5 8 4.5 4 9.5 12 13.5 20 28 30

4.5
32-35

1136.49
~~1135.77~~

53 4.3 1132.2

54 5.0 1131.5

54+19 5.2 1131.3

55 5.4 1131.1

6.79 ~~1136.89~~
~~1136.87~~ 5.39 ~~1130.10~~

56 6.6 1131.3

57 5.0 1132.9

58 5.5 1132.4

B.M. 4.22 ~~1133.67~~
~~1132.67~~

4.4 5.1 4.7 5.5 4.6 4.3 4.6 5.9 5.1 5.3 5.9 5.4
30-25 19 11 9.5 6 4 8 10.5 12 20 27 30

5.5 5.8 6.5 5.7 5.0 5.0 5.4 6.8 6.4 6.5 7.5
30-25 12 11 9 3 4 3.5 7.5 10 11 18.5 30

1128.3

6.2 7.3 6.1 5.2 5.2 5.6 7.8 8.2 9.0 9.6 10.7 11.7
30 9.2 9 3 4 6 7.0 30 60 100 150 200
FL FL

5.8 5.6 5.8 6.3 6.3 5.5 5.2 5.4 5.9 6.7 6.1 6.6 7.4
30-25 21 14 12 11.5 7.5 3 4 4.5 6 7.5 13.5 30

spike sta. 50

4.5 4.7 5.2 6.8 6.9 7.7 6.7 6.2 6.6 7.4 6.9 6.6 7.0
30 28 22 18.5 15 13.5 10.5 3.5 4 5.5 7.5 15.5 30

5.8 3.4 3.7 4.3 4.7 5.8 5.2 4.7 5.0 5.1 5.8 5.2 5.5
30-28 26 22.5 21 16 13.5 10 5.5 4 1.5 4-6 7 30

4.8 5.4 6.3 5.6 5.1 5.5 6.3 5.2 5.1
30-25 22-16 15 11 6.5 4 5 6 30

N.E. Root 30' Pine 29' Pt. Sta. 58+95

Stopped, Oct. 5, 1929
Fair 65°
Marks, Parks, Goodrich

B.M. 1.87 ~~1135.54~~ ~~1134.54~~ ~~1132.67~~ 1133.67

59 5.1 1130.4

60 12.0 1123.5
1124.47
5.12 ~~1123.47~~ 16.19 ~~1118.35~~ 1119.35

61 7.7 1116.8
1115.41
1.89 ~~1117.41~~ 10.95 ~~1112.52~~ 1113.52

62 3.1 1112.3

63 5.9 1109.5

64-1 Sta & current 6.9 1108.5

65 7.2 1108.2
1124.07
14.14 ~~1123.97~~ 5.98 ~~1108.93~~ 1109.93

66 13.6 1110.5

66+75 11.8 1112.3

N.E. 100' 30" pine 29' RT Sta. 58+85

$\frac{33}{30} \frac{3.2}{25} \frac{5.6}{15} \frac{4.4}{14} \frac{5.6}{12} \frac{7.8}{5} \frac{5.1}{2} \frac{5.6}{5.5} \frac{2.9}{9} \frac{2.3}{30}$

$\frac{6.8}{30} \frac{6.8}{25} \frac{11.3}{13.5} \frac{13.4}{12} \frac{15.6}{10.5} \frac{11.9}{5} \frac{12.0}{2} \frac{12.0}{3} \frac{12.9}{5} \frac{11.7}{7} \frac{7.1}{12} \frac{6.9}{14.5} \frac{7.6}{30}$

$\frac{3.5}{30} \frac{3.2}{25} \frac{3.2}{12.5} \frac{7.4}{13} \frac{8.4}{12} \frac{7.8}{10} \frac{7.5}{4.5} \frac{7.7}{2} \frac{8.0}{3.5} \frac{8.4}{2} \frac{7.0}{10} \frac{3.8}{2.5} \frac{2.3}{25} \frac{2.4}{30}$

$\frac{1.0}{30} \frac{1.8}{25} \frac{3.5}{12.5} \frac{4.2}{11} \frac{3.1}{9.5} \frac{2.9}{3.5} \frac{3.1}{2} \frac{3.1}{3.5} \frac{3.9}{6} \frac{3.4}{8} \frac{2.3}{12} \frac{2.7}{2.5} \frac{1.5}{30}$

$\frac{7.7}{30} \frac{7.3}{13.5} \frac{6.8}{7.5} \frac{7.2}{6.5} \frac{6.5}{5} \frac{5.9}{2} \frac{6.1}{6.5} \frac{6.6}{8-10} \frac{6.4}{10.5} \frac{7.0}{20} \frac{7.3}{30}$

$\frac{12.5}{75} \frac{12.7}{38} \frac{13.1-18}{7.6} \frac{107.6}{6.2} \frac{110.2}{6.9} \frac{110.5}{6.9} \frac{110.5}{10.69} \frac{110.4}{6.2} \frac{110.9}{8.2-13.3} \frac{110.7.2}{13.3} \frac{110.2.1}{19.7} \frac{110.2.1}{14.6} \frac{14.1}{100} \frac{15.0}{300}$

$\frac{7.7}{30} \frac{7.5}{17.5} \frac{8.9}{16.5} \frac{7.2}{12} \frac{7.0}{5.5} \frac{7.2}{4} \frac{9.1}{3} \frac{7.8}{7-9} \frac{7.5}{9.5} \frac{7.5}{17.5} \frac{7.5}{30}$

$\frac{12.2}{30} \frac{14.0}{21} \frac{14.6}{20} \frac{13.6}{16} \frac{13.3}{11.5} \frac{13.7}{3} \frac{13.6}{2} \frac{16.0}{15-3.5} \frac{14.4}{4.5} \frac{5.1}{17} \frac{5.3}{20-30}$

$\frac{11.3}{30} \frac{10.7}{15} \frac{11.7}{20} \frac{13.1}{17} \frac{12.2}{15} \frac{11.6}{9} \frac{11.8}{2} \frac{13.4}{1.5} \frac{11.6}{4} \frac{12.8}{7-9} \frac{12.3}{10} \frac{11.4}{21} \frac{10.7}{30}$

1124.07
~~1123.07~~

67 11.0 1113.1

68 8.0 1116.1

69 4.9 1119.2

1135.28
13.41 ~~1134.28~~ 2.20 ~~1129.87~~

70 12.3 1123.0

B.M. 6.86 ~~1127.42~~ 1128.42

71 8.0 1127.3

72 4.3 1131.0

1145.56
13.50 ~~1144.56~~ 3.22 ~~1131.06~~

73 11.7 1133.9

74 8.0 1137.6

74+50 6.1 1139.5

9.1 9.0 11.2 12.1 11.3 11.6 11.0 11.7 11.1 11.2 10.7
30 25 19 17 15 9 4 0.5-1.5 4 25 30

2.9 2.9 8.2 9.4 8.2 7.7 8.0 8.1 9.3 8.0 6.6 7.2 7.0
30 27 17 15 14 12.5 6 4 3 3.5 4.5 5.5 10.5 18.5 30

0.7 2.7 5.0 6.2 5.1 4.6 4.9 5.2 5.9 1.8 2.3 2.3
30 18.5 15 13-11.5 10 3.5 2 3 4.5 5.5 11 25 30

10.0 10.0 11.2 13.2 12.5 12.3 12.7 14.0 13.2 9.4 9.4
30 17.5 14.5 13-11.5 10 4 5 7.5 9 16.5 30

S. W. 1100' 20" RIME 50' left Sta. 70+50

6.0 6.8 8.9 8.1 8.0 8.6 9.8 9.0 5.9 5.7
30 15.5 13.5 12.5 10 4 6.5 8.5 9.5 15.5 30

1.8 1.5 2.3 4.8 6.1 4.7 4.3 5.2 6.0 4.9 1.2 2.7 2.8
30 23 19 13 11.5 8.5 4 7 8 9.5 15.5 17 30

10.6 11.3 10.5 12.0 12.9 12.3 11.7 11.9 13.1 12.0 10.8 10.2 9.4 9.4
30 14 14 9.5 8.5 7 4 6.5 10.5 11.5 14 17 25 30

6.0 6.8 8.3 8.8 8.2 8.0 8.8 9.5 8.9 7.4 6.9
30 14.5 11 10-8.5 6.5 4 8.5 10 11 15.5 30

4.4 5.2 7.1 6.6 6.1 6.6 7.2 7.8 7.4 6.4 5.7 6.2
30 16.5 8.5 7.5 4 5 8.5 10 11.5 16.5 17.5 20-30

1145.56
~~1147.54~~

75 6.1 1139.5

75+44 6.2 1139.4

E.M. 3.31 1142.25
1147.25

14.39 ^{1156.10}
~~1155.10~~ 5.85 1139.71
~~1138.71~~

76 16.4 1139.7

77 14.2 1141.9

78 11.4 1144.7

16.02 ^{1168.18}
~~1167.18~~ 3.94 1152.16
1151.16

79 16.0 1152.2

80 10.7 1157.5

81 8.3 1159.9

82 5.6 1162.6

3.1 5.4 6.1 7.2 6.5 6.1 6.7 7.9 7.2 7.8 7.8
30 25 15.5 10 5 4 10 11.5 20 30

^{1137.56}
3.7 6.8 7.3 8.0 6.6 6.2 7.2 8.0 8.2 8.3 8.8 9.6 11.8
~~100~~ 30 12. 8.7 8.2 4 7.1 7.6 30 50 150 250 350
_{FL.} _{FL.}

Left
R.P. Spike S.W. root 48" Locust 34.5' P+ Sta. 74100

Q spike sta. 74
16.7 16.2 17.9 16.8 16.4 17.9 17.4 17.4 17.8 17.8
30 12.5 11.5 8.5 4 8 10 15.5 16.5 30

14.2 15.2 16.1 14.6 14.2 14.9 15.8 15.0 15.0
30 12 11 7 4 7 8-9.5 11.5 30

7.6 7.6 11.4 12.9 11.9 11.7 12.1 12.6 12.1 7.3 7.3
30 18.5 14 12.5 10.5 9.5 4 7.5 9 10.5 16.5 30

11.4 11.7 11.2 15.8 17.9 16.7 16.0 14.6 17.6 16.6 12.4 12.5
30 25 18 12 9.5 8.5 4 8.5 10 10.5 17 30

8.1 9.4 8.5 11.5 12.5 14.1 14.1 10.7 11.5 12.0 8.6 8.7
26 19 12.5 12.5 11.5 11 8.5 4 9 10 14 30

5.2 6.2 8.8 10.1 9.1 8.3 8.8 9.5 9.2 6.0 6.1
30 16.5 11.5 10.5 8 4 9.5 11 12 15.5 30

3.7 3.7 6.4 7.4 6.4 5.6 6.3 6.5 5.4 4.1 4.3
30 16.5 13 11.5 9.5 4 9.5 11 12 15 30

1168.18
~~1167.18~~

82+778 2.5 1165.7

83 2.5 1165.7

83+50 2.0 1166.2

84 1.3 1166.9

84+50 0.4 1167.6

85 +0.7 1168.3

5.41 ~~1169.67~~ 2.92 ~~1167.26~~

B.M. 3.25 ~~1166.02~~

1168.95
2.13
1166.82

new B.M. 1.57 1168.10

| | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----|
| 1167.4 | 1167.0 | 1167.3 | 1167.0 | 1166.4 | 1165.3 | 1164.8 | 1163.7 | 1162.8 | 1162.1 | 23 |
| 0.8 | 1.2 | 0.9 | 1.2 | 1.8 | 2.5 | 2.9 | 3.7 | 4.5 | 5.7 | 6.1 |
| 200 | 150 | 100 | 50 | 30 | 4 | 30 | 50 | 100 | 150 | 200 |

Note Levels on Snyder's Cor. Rd were started from Stone B.M. at Snyder's Cor. Using 1238.00 E.I. Level notes of Main Market survey show this B.M. as 1235.87 (marked 1238.)

| |
|-------------|
| 1238.00 |
| 1235.87 |
| <u>2.13</u> |

Spike in telepole & Ref of Sta 110+09.9 Survey of Snyder's Cor. Rd.
R.P. spike N.W. side TRUNK 30 ^{LT} ft Sta 111

Stopped Oct 7, 1929

Farr 60°

D. Parks, R. Goodrich, C. Rand

Slope stakes July 8, 1930 Hot

D. Parks T. Snyder 90°

| | | | | |
|------|---------------------------|---------|------|---------|
| B.M. | 11.27 | 1086.32 | | 1075.05 |
| 0+30 | | | | 1075.50 |
| 1 | | | | 1078.75 |
| 2 | | | | 1082.00 |
| 3 | 11.78 | 1096.46 | 1.64 | 1084.68 |
| 3 | | | | 1085.00 |
| 4 | | | | 1088.24 |
| 5 | 12.43 | 1108.18 | 0.71 | 1095.75 |
| 5 | | | | 1093.10 |
| 6 | | | | 1099.58 |
| | 12.04 | 1120.12 | 0.10 | 1108.08 |
| 7 | | | | 1106.30 |
| 7+50 | | | | 1109.80 |
| 7+58 | flow line 8" tile 12.4 | | | 1107.5 |
| | Water flows down s. ditch | | | |
| 8 | | | | 1113.57 |
| | 11.13 | 1127.20 | 4.05 | 1116.07 |
| 8+50 | | | | 1117.64 |
| 9+00 | | | | 1122.00 |

| | | | |
|-------|------------------------------|---------------------|---------------------|
| X on | S.E. Corner, south Headwall, | | Culvert 0+20 |
| | | $\frac{F0.4}{25.0}$ | $\frac{F1.8}{24.0}$ |
| 10.82 | 11.26 | | 12.62 |
| | | $\frac{C0.3}{22.5}$ | $\frac{F0.6}{22.5}$ |
| 7.57 | 7.29 | | 8.15 |
| | | $\frac{F0.6}{21.5}$ | $\frac{F0.5}{19.0}$ |
| 4.32 | 4.95 | | 4.80 |
| | | $\frac{C0.7}{22.5}$ | $\frac{F0.3}{24.0}$ |
| 11.46 | 10.76 | | 11.78 |
| | | $\frac{C2.8}{26.0}$ | $\frac{C1.2}{23.5}$ |
| 8.22 | 5.43 | | 7.02 |
| | | $\frac{C3.8}{29.5}$ | $\frac{C2.4}{26.5}$ |
| 15.08 | 11.25 | | 12.70 |
| | | $\frac{C4.9}{30.0}$ | $\frac{C2.0}{21.5}$ |
| 8.60 | 3.82 | | 4.64 |
| | | $\frac{C3.4}{27.0}$ | $\frac{F0.9}{21.0}$ |
| 13.82 | 10.45 | | 14.71 |
| | | $\frac{C2.0}{25.5}$ | $\frac{F1.6}{24.0}$ |
| 10.32 | 8.29 | | 11.89 |
| | | $\frac{C5.4}{29.0}$ | $\frac{F2.0}{22.5}$ |
| 6.55 | 1.19 | | 8.51 |
| | | $\frac{C9.1}{33.0}$ | $\frac{F1.6}{23.0}$ |
| 9.56 | 0.46 | | 11.13 |
| | | $\frac{C1.6}{22.0}$ | $\frac{C1.6}{22.0}$ |
| 5.20 | | | 3.65 |

1127.20

B.M.

11.76 1115.44

11.76 1127.20 1115.50 record

10.39 1137.19 0.46 1126.80

9 1122.00 15.19 5.39

$\frac{C9.8}{33.0}$

10 7.41 1144.30 0.30 1136.89

6.9

10 1130.50 13.80 7.41

$\frac{C6.4}{32.0}$

12.95

$\frac{C0.9}{19.0}$

11 1136.50 7.80 4.50

$\frac{C3.3}{27.0}$

6.54

$\frac{C1.3}{25.0}$

7.83 1149.79 2.34 1141.96

12 1141.62 8.17 4.23

$\frac{C3.9}{28.5}$

7.22

$\frac{C1.0}{21.0}$

13 1146.00 3.79 1.77

$\frac{C2.0}{25.5}$

2.22

$\frac{C1.6}{25.0}$

9.63 1158.72 0.70 1149.09

14 1149.90 8.82 5.94

$\frac{C2.9}{22.5}$

7.51

$\frac{C1.3}{24.5}$

15 1153.10 5.62 4.14

$\frac{C1.5}{24.5}$

7.31
1151.41

$\frac{F1.7}{21.5}$

12.75 1164.82 6.65 1152.07

16 1155.60 9.22 6.14

$\frac{C3.1}{27.5}$

8.77

$\frac{C0.5}{23.5}$

B.M. 8.31 1156.51

1156.55 record

(record 1115.50)
spike, N.W. root 20" Maple, 30' Rt. sta, 8+30

16+50

July 17-30
 Marks
 C. Parks.

Fair - 80°

27

| | | | | | | | | | |
|-------|------|---------|------|---------|-------|-------|---|-------|----------------------|
| B.M. | 9.19 | 1165.74 | | 1156.55 | | | | | |
| 16+50 | | | | 1156.80 | 8.94 | 4.54 | <u>C4.4</u> 29.5 | 7.71 | <u>C1.2</u> 25.0 |
| 17 | | | | 1157.90 | 7.78 | 4.02 | <u>C3.8</u> 28.0 | 6.82 | <u>C0.9</u> 24.0 |
| +62.1 | | | | 1159.00 | 6.74 | 6.52 | <u>C0.2</u> 22.5 | 7.93 | <u>F1.2</u> 22.0 |
| 18 | | | | 1159.60 | 6.14 | 5.31 | <u>C0.8</u> 24.0 | 6.00 | <u>C0.1</u> 22.5 |
| 19 | | | | 1161.20 | 4.54 | 3.14 | <u>C1.4</u> 24.5 | 4.90 | <u>F0.4</u> 22.5 |
| T.P. | 9.50 | 1172.53 | 0.69 | 1165.05 | | | | | |
| 20 | | | | 1162.00 | 10.55 | 7.50 | <u>C3.0</u> 17.0 | 9.14 | <u>C1.4</u> 24.5 |
| +50 | | | | 1162.00 | 10.55 | 6.95 | <u>C3.6</u> 23.5 | 8.12 | <u>C2.4</u> 21.5 |
| 21 | | | | 1162.00 | 10.55 | 6.02 | <u>C4.5</u> 29.0 | 8.81 | <u>C1.7</u> 26.5 |
| +50 | | | | 1162.00 | 10.55 | 8.39 | <u>C1.2</u> 25.5 | 14.95 | <u>F4.4</u> 26.5 |
| 22 | | | | 1162.00 | 10.55 | 13.05 | <u>F2.5</u> 22.0 | 14.49 | <u>F3.5</u> 25.0 |
| 23 | | | | 1163.60 | 8.95 | 3.47 | <u>C5.5</u> 29.0 | 7.73 | <u>C1.2</u> 26.0 |
| T.P. | 9.45 | 1178.53 | 3.47 | 1169.08 | | | | | |
| 24 | | | | 1166.80 | 11.73 | 6.05 | Hub Left Sta. 23 <u>C5.7</u> 30.0 | 10.52 | <u>C1.2</u> 26.0 |
| 25 | | | | 1170.00 | 8.53 | 6.11 | <u>C2.4</u> 26.5 | 10.69 | <u>F.2.2</u> 21.0 |

1178.53

| | | | | | | | | | |
|-------|------|---------|-------|---------|------|------|---------------------|------|----------------------|
| 26 | | | | 1172.50 | 6.03 | 5.26 | $\frac{C0.8}{24.0}$ | 7.63 | $\frac{F1.6}{23.5}$ |
| T.P. | 7.70 | 1184.10 | 2.13 | 1176.40 | | | | | |
| 27 | | | | 1175.00 | 9.10 | 4.65 | $\frac{C4.5}{28.5}$ | 8.97 | $\frac{C0.1}{22.0}$ |
| 28 | | | | 1177.50 | 6.60 | 2.56 | $\frac{C4.0}{28.0}$ | 5.74 | $\frac{C0.9}{24.0}$ |
| +75 | | | | 1178.47 | 5.62 | 1.62 | $\frac{C4.0}{23.5}$ | 5.62 | $\frac{C0.0}{30.00}$ |
| 29 | | | | 1178.38 | 5.71 | 2.00 | $\frac{C3.7}{23.0}$ | 5.03 | $\frac{C0.7}{25.0}$ |
| B.M. | | | 1.04 | 1183.06 | | | | | |
| | 404 | 1184.09 | | 1183.05 | | | | | |
| 29+50 | | | | 1177.60 | 6.49 | 2.27 | $\frac{C4.2}{28.0}$ | 6.10 | $\frac{C0.4}{23.0}$ |
| 30 | | | | 1176.00 | 8.09 | 3.54 | $\frac{C4.6}{29.0}$ | 8.42 | $\frac{F0.3}{23.0}$ |
| | 432 | 1177.54 | 10.89 | 1173.22 | | | | | |
| 30+50 | | | | 1174.00 | 3.54 | 2.33 | $\frac{C1.2}{24.0}$ | 3.95 | $\frac{F0.4}{22.0}$ |
| 31 | | | | 1172.37 | 5.17 | 5.01 | $\frac{C0.2}{22.5}$ | 7.34 | $\frac{F2.2}{21.0}$ |
| 32 | | | | 1170.96 | 6.58 | 4.41 | $\frac{C2.1}{25.0}$ | 7.58 | $\frac{F1.0}{20.0}$ |

B.M. S. root 20" maple 30' left 28 + 47

| | | | | | | | | | |
|-------|------|---------|-------|---------|-------|----------------------------|--|-----------------------------|---------------------|
| T.P. | 130 | 1174.52 | 432 | 1173.22 | | | | | |
| 33 | | | | 1169.92 | 4.60 | 2.48 | $\frac{C2.2}{26.0}$ | 7.68 | $\frac{F2.9}{23.5}$ |
| 33+50 | | | | 1169.53 | 4.99 | ^{1168.63} 5.89 | $\frac{F}{21.5}$ 20.9 | 8.15 | $\frac{F3.2}{24.0}$ |
| 34 | | | | 1169.40 | 5.12 | 0.16 | $\frac{C5.0}{}$ | 5.61 | $\frac{F0.5}{19.5}$ |
| T.P. | 995 | 1179.29 | 518 | 1169.39 | | | | | |
| 34+50 | | | | 1169.05 | 10.24 | 5.08 | $\frac{C5.2}{30.0}$ | 10.65 | $\frac{F0.4}{23.0}$ |
| 35 | | | | 1167.90 | 11.39 | 6.49 | $\frac{C4.9}{30.0}$ | 10.97 | $\frac{C0.4}{23.5}$ |
| 35+50 | | | | 1166.00 | 13.29 | 7.72 | $\frac{C5.6}{31.0}$ | 12.49 | $\frac{C0.8}{24.0}$ |
| 36 | | | | 1163.40 | 15.89 | 9.26 | $\frac{C6.6}{33.0}$ | 13.32 | $\frac{C2.6}{28.0}$ |
| T.P. | 8.38 | 1169.35 | 13.32 | 1165.97 | | | | | |
| 36+50 | | | | 1160.40 | 8.95 | 5.45 | Slope hub right $\frac{C3.5}{27.0}$ | 36+00 9.28 | $\frac{F0.3}{24.5}$ |
| 37 | | | | 1158.10 | 11.25 | 10.82 | $\frac{C0.4}{23.0}$ | 14.65 | $\frac{F3.4}{23.5}$ |
| 38 | | | | 1156.95 | 12.40 | 13.88 | $\frac{F1.5}{21.0}$ | 1154.87 14.48 | $\frac{F2.1}{22.0}$ |

R. Hassel - chuf
E. Parks asst.

Fair - Hot,

30

| | | | | | | | | | |
|-------|------|----------|------|---------|---------------------------------|-------|---------------------|-------|--------------------------------|
| 39 | | 11.09.35 | | 1157.11 | 12.24 | 12.45 | $\frac{F0.2}{22.0}$ | 10.70 | $\frac{C1.5}{24.5}$ |
| 40 | | | | 1158.50 | 10.85 | 9.90 | $\frac{C1.4}{25.0}$ | 8.76 | $\frac{C2.1}{26.0}$ |
| T.P. | 9.09 | 1169.09 | 9.90 | 1159.95 | slope Hub on Lt. 520 | | 40. | | |
| 41 | | | | 1160.50 | 8.54 | 7.71 | $\frac{C0.8}{24.0}$ | 6.40 | $\frac{C2.1}{25.5}$ |
| 42 | | | | 1162.50 | 6.54 | 6.18 | $\frac{C0.4}{23.0}$ | 4.75 | $\frac{C1.8}{25.5}$ |
| 43 | | | | 1164.50 | 4.54 | 3.44 | $\frac{C1.1}{24.0}$ | 3.45 | $\frac{C1.1}{25.0}$ |
| T.P. | 4.62 | 1170.29 | 3.35 | 1165.67 | slope Hub on Rt side 44. | | | | |
| +76.6 | | | | 1165.90 | - cross road. | | | | |
| 44 | | | | 1166.00 | 4.29 | 3.33 | $\frac{C0.9}{24.0}$ | 4.62 | $\frac{F0.4}{23.0}$ Lt. +60 |
| B.M. | 0.70 | 1170.39 | 0.70 | 1169.59 | R.P. spike S.E. side 27" Walnut | | | | |
| 45 | | | | 1169.64 | record | | | | |
| | | | | 1163.70 | 6.64 | 2.25 | $\frac{C4.4}{29.0}$ | 4.00 | $\frac{C2.6}{27.5}$ |
| +50 | | | | 1161.00 | 9.34 | 4.42 | $\frac{C4.9}{30.0}$ | 5.73 | $\frac{C3.6}{29.0}$ |
| 46. | | | | 1157.75 | 12.59 | 9.92 | $\frac{C3.1}{27.5}$ | 9.84 | $\frac{C2.8}{26.5}$ |

1170.34

| | | | | | | | | | |
|-------|------|---------|-------|---------|-------|-------|---|-----------------|---------------------|
| 46+50 | | | | 1154.50 | 15.84 | 14.51 | $\frac{C1.3}{24.0}$ | 15.80 | $\frac{C0.1}{24.0}$ |
| T.P. | 3/3 | 1137.34 | 16.13 | 1154.21 | | | | | |
| 47 | | | | 1151.25 | 6.09 | 4.50 | $\frac{C1.6}{24.5}$ | 5.12 | $\frac{C1.0}{24.0}$ |
| 750 | | | | 1148.00 | 9.34 | 7.22 | $\frac{C2.1}{24.5}$ | 8.43 | $\frac{C0.9}{24.5}$ |
| 48 | | | | 1144.75 | 12.59 | 10.10 | $\frac{C2.5}{26.0}$ | 11.09 | $\frac{C1.5}{25.0}$ |
| 49 | | | | 1140.25 | 12.09 | 15.29 | $\frac{C1.8}{25.0}$ | 16.08 | $\frac{C1.0}{25.0}$ |
| T.P. | 126 | 1143.81 | 15.29 | 1142.05 | | | | | |
| 50 | | | | 1137.75 | 6.06 | 6.40 | Hub m. Lt. - 49 $\frac{F0.4}{32.0}$ | 6.45 | $\frac{F0.4}{23.5}$ |
| 51 | | | | 1135.25 | 8.56 | 8.94 | $\frac{F0.4}{32.0}$ | 9.04 | $\frac{F0.5}{20.0}$ |
| T.P. | 2.81 | 1137.68 | 8.94 | 1134.87 | | | | | |
| 52 | | | | 1133.50 | 4.18 | 4.49 | LT side 51 - on Hub, $\frac{F0.3}{32.0}$ | 4.93 | $\frac{F0.8}{20.0}$ |
| 53 | | | | 1132.50 | 5.18 | 5.51 | $\frac{F0.3}{31.5}$ | 6.05 | $\frac{F0.9}{20.0}$ |
| 54 | | | | 1131.50 | 6.18 | 6.58 | $\frac{F0.4}{31.5}$ | 1129.90 7.78 | $\frac{F1.6}{20.5}$ |

1137.65

55 1131.00

6.68 5.60 $\frac{C1.0}{31.5}$ 8.00 $\frac{F1.3}{20.5}$

56 1131.50

6.56 Lt 4.45 $\frac{C2.1}{33.0}$ 6.18 rz 6.44 $\frac{F0.3}{23.0}$

T.P. 6.82 1138.06 6.44 1131.24

* Hub in Pt. Sta. 56, $\frac{C2.0}{25.5}$ 5.92 $\frac{C0.1}{23.5}$

57 1132.50

5.56 3.60 $\frac{F0.1}{22.5}$ 5.36 $\frac{F0.3}{23.0}$

58 1133.03

5.03 3.17 $\frac{C2.1}{24.5}$ 4.95 $\frac{C2.8}{27.5}$

59 1130.33

7.73 5.33 $\frac{C.5.2}{29.5}$ 5.86 $\frac{C4.0}{27.0}$

B.M. 0.54 1134.21 4.42 1133.67 record

Front 30" pine rz of Sta. 59

60 1124.40

9.81 4.62 $\frac{C4.3}{28.0}$ 5.9 $\frac{C3.5}{27.5}$

T.P. 4.68 1127.40 11.49 1122.72

61 1118.00

9.40 5.15 $\frac{C2.0}{25.5}$ 3.11 $\frac{C2.3}{24.5}$

T.P. 1.53 1117.67 11.26 1116.14

62 1112.26

5.41 3.43 $\frac{F2.2}{23.0}$ 9.15 $\frac{F2.0}{22.0}$

63 1110.50

7.17 9.40

8.35

64 1109.54

Bridge.

| | | | | |
|------|-------|---------|------|----------------|
| T.P | 11.84 | 1121.16 | 8.35 | 1109.32 |
| 65 | | | | 1109.55 |
| 66 | | | | 1110.75 |
| +75 | | | | 1112.44 |
| T.P. | 15.39 | 1128.15 | 8.40 | 1112.76 |
| 67 | | | | 1113.15 |
| 68 | | | | 1116.60 |
| 69 | | | | 1120.20 |
| 70 | | | | 1123.80 |
| T.P. | 6.17 | 1132.16 | 2.16 | 1125.99 |
| BM | | | 3.68 | 1128.48 |
| | | | | 1128.42 record |

| | | | | |
|--|-------|---------------------|-------|---------------------|
| 11.61 | 13.20 | $\frac{F1.6}{21.0}$ | 13.25 | $\frac{F1.6}{21.0}$ |
| 10.41 | | $\frac{F0.8}{18.5}$ | 2.24 | $\frac{C8.2}{32.0}$ |
| 8.72 | 7.8 | $\frac{C0.9}{23.0}$ | 8.40 | $\frac{C0.3}{23.0}$ |
| Slope Hub. Right 66+75 July 31, 1930, Fair 25° Marks, Parks | | | | |
| 15.00 | 14.2 | $\frac{C0.8}{23.0}$ | 15.04 | $\frac{0.0}{22.5}$ |
| 11.55 | 7.00 | $\frac{C4.5}{30.0}$ | 11.25 | $\frac{C0.3}{24.0}$ |
| 7.95 | 5.08 | $\frac{C2.9}{25.5}$ | 6.61 | $\frac{C1.3}{26.0}$ |
| 4.35 | 2.15 | $\frac{C2.2}{25.5}$ | 2.23 | $\frac{C2.1}{26.0}$ |

S. W. T. 20" Pine Lt 572 70 + 50

| | | | | |
|-------|-------|---------|------|---------|
| BM | 9.00 | 1137.42 | | 1128.42 |
| 71 | | | | 1127.40 |
| 72 | | | | 1131.00 |
| 73 | | | | 1134.60 |
| T.P. | 9.35 | 1144.94 | 2.43 | 1134.99 |
| 74 | | | | 1138.00 |
| 74+50 | | | | 1139.10 |
| | | | 2.11 | 1142.33 |
| B.M. | 2.11 | 1144.36 | | 1142.25 |
| 75 | | | | 1139.80 |
| 76 | | | | 1140.00 |
| 77 | | | | 1141.50 |
| T.P. | 15.14 | 1159.50 | 0.00 | 1144.36 |
| 78 | | | | 1146.00 |

| | | | | |
|----------------------------|-------|---------|-------|-------|
| 5, W. root 20" Pine 50'L - | 70+50 | | | |
| | | C 1.8 | | C 2.3 |
| 10.02 | 8.21 | 25.0 | 7.72 | 26.0 |
| 6.42 | 3.69 | C 2.8 | | C 2.0 |
| | | 27.5 | 4.19 | 25.5 |
| 2.82 | 2.48 | C 0.4 | | C 1.7 |
| | | 25.0 | 1.15 | 24.0 |
| 6.44 | 4.94 | C 1.5 | | C 0.9 |
| | | 24.5 | 5.59 | 24.5 |
| 5.34 | 3.10 | C 2.2 | | C 0.6 |
| | | 25.5 | 4.72 | 24.0 |
| 5, W. root 48" Locust | 74+55 | | | - Lt. |
| | | 1140.07 | | F 2.3 |
| 4.56 | 4.29 | C 0.3 | | 22.0 |
| | | 23.0 | 6.90 | |
| 4.36 | 5.19 | F 0.8 | | F 1.9 |
| | | 22.0 | 6.29 | 21.5 |
| 2.86 | 2.84 | 0.0 | | F 0.5 |
| | | 22.5 | 3.30 | 23.0 |
| Peg in ditch line | | | | |
| 13.50 | 10.60 | C 2.9 | | C 2.6 |
| | | 26.5 | 10.90 | 27.5 |

1159.50

79

1152.00

7.50

2.62

 $\frac{0.49}{30.0}$

3.99

 $\frac{0.35}{29.5}$

11.54 1169.42 1.62 1157.88

80

1157.12

12.30

9.23

 $\frac{0.31}{26.5}$

9.85

 $\frac{0.25}{27.5}$

81

1160.50

8.92

6.88

 $\frac{0.21}{26.0}$

7.41

 $\frac{0.45}{26.0}$

82

1163.00

6.42

4.54

 $\frac{0.19}{25.5}$

5.41

 $\frac{0.10}{24.5}$

4 Snyder's Rd.
+ 77.8

3.68

1165.74

1165.70

3.72

3.68

0.31

1169.11

R.R spike

N.W. side trunk - 20" diam. - 83+25± - Lt.

B.M.

Aug. 2, 1930, Fair-850
Marks, E. A. Parks.

14+93, 15" Corr. Iron. Pipe Culvert
42' long

15+00 5.06 1156.47 1151.41

14+93 1152.9

5.22 1149.75

0.22 1151.25

17+62 15' Corr. Iron Pipe Culvert, 36' long

17+62 1159.00

5.13 1164.35 1159.22

3.71 1157.14

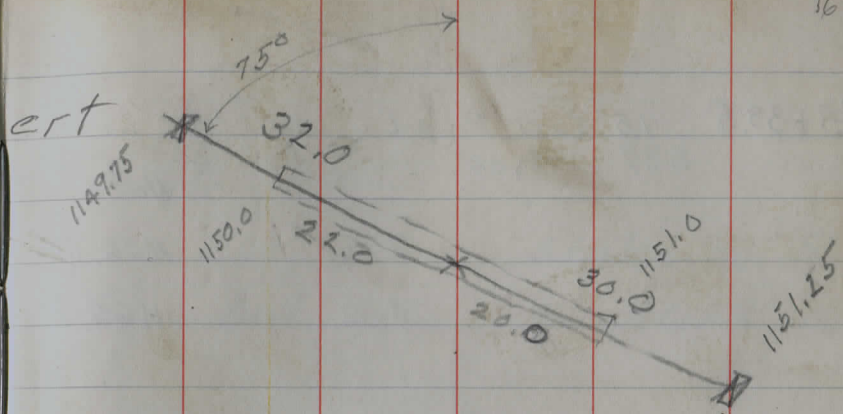
5.49 1156.36

21+83 15" Corr. Pipe Culvert 40' long

7.94 1165.54 1162.0

4.54 1157.60 1158.5

7.04 1157

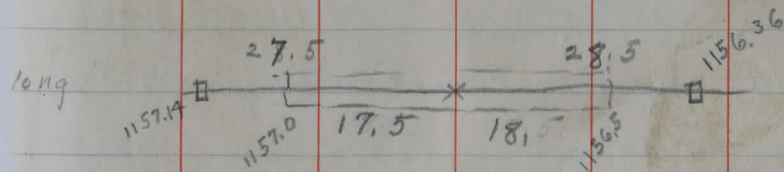


Slope Hub, R. 15+00

Sub grade at \pm

6.72 Cut 1'6" Stake 32' R.

5.22 Cut 5'-0" Stake 30' L.



Subgrade at \pm

Slope Hub, Left 17+62

7.21 Cut 3'6" Stake 27.5' L

7.99 Cut 2'6" Stake 28.5' R.



Subgrade at \pm

Slope Hub 21+50 R.

7.04 Cut 2'6" Stake 29' L

8.04 Cut 1'0" Stake 31' R.

33+33.5 15" Corr. Pipe Culvert 40' Long
 5.37 1174.00 1168.63
 1169.6
 7.0 1166.5
 4.0 1167.5

Hub, Left 33+50
 Subgrade at £
 7.5 Cut 6" Stake 31' R.
 6.5 Cut 2'6" Stake 29' L.

37+82, 24" Corr Pipe Culvert 40' Long
 6.46 1161.33 1157.00
 1154.87
 5.83 1152.5
 3.83 1153.5
 3.78 1133.68 1129.90

Subgrade at £.
 Hub, 38+00 Right.
 8.83 Cut 3' Stake 31' R.
 7.83 Cut 4' Stake 29' L.
 Aug. 14, Cloudy, 75° SE Wind,
 Marks + Snyder.
 Slope Hub, 54+00, R.

54+19 15" Corr. Pipe Culvert 36' Long
 1131.30
 2.90 1128.30
 1.90 1129.30
 3.01 1143.08 1140.07

Subgrade at £.
 5.38 Cut 2'6" Stake 29' R.
 4.38 Cut 2'6" Stake 27' L.

75+44 Culvert, 36' of 15" Corr Pipe 1140.00
 3.28 1137.80
 4.28 1137.30

Slope Hub, 75+00, R.
 Subgrade at £.
 5.28 Cut 2' Stake 27' L.
 5.78 Cut 1'6" Stake 29' R.

Aug. 29, 1930 D. Parks
 Hot 80° R. Hassel

| | | | | |
|-------|------|---------|-------|---------|
| B.M. | 0.08 | 1169.18 | | 1169.10 |
| 82 | | | | 1163.00 |
| 81 | | | | 1160.50 |
| 80 | | | | 1157.12 |
| 79 | 1.58 | 1157.90 | 12.86 | 1156.32 |
| 78 | | | | 1152.00 |
| 77 | | | | 1146.00 |
| 76 | 0.12 | 1145.26 | 12.76 | 1145.14 |
| 75 | | | | 1141.50 |
| 74 | | | | 1140.00 |
| 73 | | | | 1139.80 |
| 74+50 | | | | 1139.10 |

R.P. & B.M. spike N.W. side of trunk, 20" Elev

| | | | | | |
|-------|-------------------------|-------------------|------------------|-------------------|-------------------------|
| 6.18 | Back slope 3.0 scant | $\frac{6.6}{15}$ | $\frac{6.4}{4}$ | $\frac{6.4}{15}$ | Back slope 1.8 scant |
| 8.48 | Back slope 4.0 scant | $\frac{9.1}{15}$ | $\frac{9.1}{4}$ | $\frac{8.7}{15}$ | Back slope 3.9 scant |
| 12.06 | Back slope 3.3 scant | $\frac{12.1}{15}$ | $\frac{11.8}{4}$ | $\frac{11.4}{15}$ | Back slope 5.8 scant |
| 5.90 | Back slope 8.0 scant | $\frac{5.6}{15}$ | $\frac{5.5}{4}$ | $\frac{5.3}{15}$ | Back slope 8.0 scant |
| 11.90 | Back slope 4.1 scant | $\frac{12.7}{15}$ | $\frac{12.7}{4}$ | $\frac{12.2}{15}$ | Back slope 5.0 scant |
| 3.76 | Back slope 1.0 scant | $\frac{3.7}{15}$ | $\frac{3.4}{4}$ | $\frac{3.7}{15}$ | Back slope 1.8 scant |
| 5.26 | Back slope | $\frac{5.5}{15}$ | $\frac{5.4}{4}$ | $\frac{6.1}{15}$ | |
| 5.46 | | $\frac{5.8}{15}$ | $\frac{5.8}{4}$ | $\frac{6.6}{15}$ | Back slope 0.7 scant |
| 6.16 | Back slope 3.0 scant | $\frac{6.2}{15}$ | $\frac{6.0}{4}$ | $\frac{6.6}{15}$ | Back slope 2.0 scant |

1145.26

B.M. 2.97 1142.29
 2.97 1145.22 1142.25 record
 74 1138.00
 T.P. 10.96 1134.26

B.M. 1.81 1144.06 1142.25
 75+44

T.P. 0.59 1134.85 1134.26
 73 1134.60

72 1131.00

71 1127.40

70 1123.80

S. W. root 24" Locust

Back slope $\frac{7.9}{15}$ $\frac{7.6}{15}$ $\frac{8.0}{15}$ Back slope
 7.22 2.4 scant 2.6 scant
 Stone Rt sta 73

6.3 6.7

1137.8 1137.4

Length of Corr. pipe Culvert 36.04

Back slope $\frac{0.9}{15}$ $\frac{0.6}{15}$ $\frac{0.6}{10}$ Back slope
 0.15 1.8 scant 3.5 scant

Back slope $\frac{3.8}{15}$ $\frac{3.6}{15}$ $\frac{3.3}{15}$ Back slope
 3.85 5.0 scant 3.0 scant

Back slope $\frac{7.3}{15}$ $\frac{7.2}{15}$ $\frac{7.3}{15}$ Back slope
 7.45 1.5 scant 4.5 scant

Back slope $\frac{11.5}{15}$ $\frac{10.9}{15}$ $\frac{11.4}{15}$ Back slope
 11.05 2.5 scant 5.0 scant

1134.85

6.14 1128.73 12.26 1122.59

B.M. 0.30 1128.43

0.30 1128.72 1128.42 record

69 1120.20

68 1114.60

2.04 1118.18 12.58 1116.14

67 1113.15

66 1110.75

65 1109.55

T.P. 8.27 1109.91

S.W. root 20" pine 50' Lt. sta. 70+50

| | | | | | |
|------|------------|-----|-----|-----|------------|
| | Back slope | 8.9 | 8.5 | 8.4 | Back slope |
| 8.52 | 2.6 scant | 15 | 4 | 15 | 4.0 scant |

| | | | | | |
|-------|------------|-------|------|------|------------|
| | Back slope | 9.2.5 | 12.2 | 12.2 | Back slope |
| 12.58 | 7.0 scant | 15 | 4 | 15 | 1.8 scant |

| | | | | | |
|------|------------|-----|-----|-----|------------|
| | Back slope | 4.8 | 4.9 | 4.9 | Back slope |
| 5.13 | scant | 15 | 4 | 15 | 2.0 scant |

| | | | | |
|------|--|-----|-----|-----|
| | | 7.1 | 7.0 | 6.0 |
| 7.43 | | 15 | 4 | 15 |

| | | | | |
|------|--|-----|-----|-----|
| | | 9.6 | 9.6 | 9.1 |
| 9.63 | | 15 | 4 | 15 |

X on S.E. corner E. Wall of Bridge

Sept. 6, 1930

D. Parks
R.L. Hassel

41

clear 80°

| | | | | |
|------|------|---------|-------|---------|
| B.M. | 0.25 | 1169.35 | | 1169.10 |
| 82 | | | | 1163.00 |
| 81 | | | | 1160.50 |
| 80 | | | | 1157.12 |
| | 0.36 | 1156.71 | 12.80 | 1156.55 |
| 79 | | | | 1152.00 |
| | 0.74 | 1149.63 | 8.02 | 1148.89 |
| 78 | | | | 1146.00 |
| 77 | | | | 1141.50 |
| 76 | | | | 1140.00 |
| 75 | | | | 1139.80 |
| | 1.91 | 1143.17 | 8.37 | 1141.26 |
| B.M. | | 0.88 | | 1142.29 |

R.P. + B.M. spike N.W. side of trunk, 20" dia

| | | | | | |
|------|------------|------------------|------------------|------------------|------------|
| 6.35 | Back slope | $\frac{7.2}{15}$ | $\frac{6.6}{15}$ | $\frac{6.6}{15}$ | Back slope |
| | 2.3 scant | | | | 1.0 scant |

| | | | | | |
|------|------------|------------------|------------------|------------------|------------|
| 8.85 | Back slope | $\frac{9.3}{15}$ | $\frac{9.0}{15}$ | $\frac{9.0}{15}$ | Back slope |
| | 2.0 scant | | | | 2.3 scant |

| | | | | | |
|-------|------------|-------------------|-------------------|-------------------|------------|
| 12.23 | Back slope | $\frac{11.9}{15}$ | $\frac{11.9}{15}$ | $\frac{12.0}{15}$ | Back slope |
| | 1.0 scant | | | | 3.7 scant |

| | | | | | |
|------|------------|------------------|------------------|------------------|------------|
| 4.91 | Back slope | $\frac{4.6}{15}$ | $\frac{4.1}{15}$ | $\frac{4.2}{15}$ | Back slope |
| | 4.0 scant | | | | 5.0 scant |

| | | | | | |
|------|------------|------------------|------------------|------------------|------------|
| 3.63 | Back slope | $\frac{4.3}{15}$ | $\frac{3.7}{15}$ | $\frac{4.0}{15}$ | Back slope |
| | 1.5 scant | | | | 4.0 scant |

| | | | | | |
|------|------------|------------------|------------------|------------------|------------|
| 8.13 | Back slope | $\frac{8.8}{15}$ | $\frac{7.9}{15}$ | $\frac{8.4}{15}$ | Back slope |
| | 1.0 scant | | | | 1.0 scant |

| | | | | | |
|------|--|-------------------|------------------|-------------------|--|
| 9.63 | | $\frac{10.1}{15}$ | $\frac{9.8}{15}$ | $\frac{10.7}{15}$ | |
|------|--|-------------------|------------------|-------------------|--|

| | | | | | |
|------|--|-------------------|-------------------|-------------------|--|
| 9.83 | | $\frac{10.7}{15}$ | $\frac{10.2}{15}$ | $\frac{11.2}{15}$ | |
|------|--|-------------------|-------------------|-------------------|--|

S.W. root 48" Locust

B.M. 0.88 1143.13

1142.25

7450

1139.10

74

1138.00

73

1134.60

0.66 1135.67 10.12 1133.01

72

1131.00

71

1127.40

B.M.

(1128.42 record)
5.25 1128.42

70

1123.80

1.91 1123.42 12.16 1121.51

69

1120.20

68

1116.00

S.W. root 48" Locust

Back slope $\frac{4.3}{15}$ $\frac{3.9}{\cancel{15}}$ $\frac{4.7}{15}$ Back slope
4.03 1.0 scant

Back slope $\frac{5.7}{15}$ $\frac{5.5}{\cancel{15}}$ $\frac{5.9}{15}$ Back slope
5.13 1.0 scant

Back slope $\frac{9.2}{15}$ $\frac{8.9}{\cancel{15}}$ $\frac{9.1}{15}$ Back slope
8.53 1.0 scant

Back slope $\frac{2.7}{15}$ $\frac{2.2}{\cancel{15}}$ $\frac{2.1}{15}$ Back slope
2.67 4.0 scant

Back slope $\frac{6.0}{15}$ $\frac{5.8}{\cancel{15}}$ $\frac{6.1}{15}$ Back slope
6.27 2.0 scant

(recorded)
S.W. root 20" pine 50' lt. sta. 70+50

Back slope $\frac{10.3}{15}$ $\frac{9.7}{\cancel{15}}$ $\frac{10.0}{15}$ Back slope
9.87 2.0 scant

Back slope $\frac{3.5}{15}$ $\frac{3.0}{\cancel{15}}$ $\frac{3.1}{15}$ Back slope
3.22 1.0 scant

Back slope $\frac{7.1}{15}$ $\frac{6.7}{\cancel{15}}$ $\frac{7.1}{15}$
4.82 3.0 scant

1123.42

| | | | | | | | | | |
|-------|------------------------------|---------|-------|---------|-------|-------------------------|----------------------------|---------------------------|--|
| 67 | | | | 1113.15 | 10.27 | $\frac{10.3}{15}$ | $\frac{9.8}{\cancel{15}}$ | $\frac{10.5}{15}$ | |
| | 1.84 | 1113.71 | 11.55 | 1111.87 | | | | | |
| 66 | | | | 1110.75 | 2.96 | $\frac{2.7}{15}$ | $\frac{2.1}{\cancel{15}}$ | $\frac{2.1}{15}$ | |
| 65 | | | | 1109.55 | 4.16 | $\frac{5.5}{15}$ | $\frac{4.7}{\cancel{15}}$ | $\frac{5.0}{15}$ | |
| 64 | | | | 1109.54 | 4.17 | $\frac{4.3}{15}$ | $\frac{4.3}{\cancel{15}}$ | $\frac{4.5}{15}$ | |
| 64+01 | Concrete extension of Bridge | | | | 30.4 | open roadway | | 32.0 | overall length |
| | 12.51 | 1121.10 | 5.12 | 1108.59 | | | | | |
| 63 | | | | 1110.50 | 10.60 | $\frac{12.6}{12}$ | $\frac{10.9}{\cancel{15}}$ | $\frac{11.3}{15}$ | |
| 62 | | | | 1112.26 | 8.84 | Back slope 4.0 scant | $\frac{8.9}{15}$ | $\frac{8.3}{\cancel{15}}$ | $\frac{9.0}{15}$ Back slope 3.0 scant |
| 61 | | | | 1118.00 | 3.10 | Back slope 4.0 scant | $\frac{3.5}{15}$ | $\frac{3.1}{\cancel{15}}$ | $\frac{3.0}{15}$ Back Slope 3.0 scant |
| | 12.31 | 1132.74 | 0.67 | 1120.73 | | | | | |
| 60 | | | | 1124.40 | 8.34 | Back slope 3.0 scant | $\frac{8.4}{15}$ | $\frac{8.0}{\cancel{15}}$ | $\frac{7.9}{15}$ Back slope 3.0 scant |
| | 4.74 | 1136.12 | 1.36 | 1131.38 | | | | | |
| B.M. | | | 2.42 | 1133.70 | | | | | |
| | | | | 1133.67 | | | | | record |
| | | | | | | | | | E. root 30" pine |

Sept 15, 1930
 O. Parks
 E. Hassel
 J. England

| | | | | |
|------|------|---------|-------|-----------------|
| B.M | 0.58 | 1169.48 | | 1169.10 |
| 82 | | | 4.7 | 1163.00 1163.00 |
| 81 | | | | 1160.50 |
| T.P. | 3.90 | 1160.79 | 12.79 | 1156.89 |
| 80 | | | | 1157.12 |
| 79 | | | | 1152.00 |
| T.P. | 1.34 | 1150.18 | 11.95 | 1148.84 |
| 78 | | | | 1146.00 |
| 77 | | | | 1141.50 |
| 76 | | | | 1140.00 |
| T.P. | 4.59 | 1143.21 | 11.56 | 1138.62 |
| 75 | | | | 1139.80 |
| B.M | | | 1.02 | 1142.19 |
| | 1.02 | 1143.27 | | 1142.25 Record |

N S

R.P.+B.M. Spike N.W. side of trunk, 20" Elm

1163.00

| | | | | | | | |
|------|-----|-----|-----|-----|------|-----|-----|
| 6.68 | 3.2 | 8.4 | 6.8 | 6.7 | 6.9 | 8.0 | 5.8 |
| | 23 | 18 | 13 | 15 | 19.5 | 23 | |

1160.5

| | | | | | | | |
|------|------|------|------|------|------|-------|-----|
| 9.18 | 7.7 | 10.4 | 9.2 | 9.2 | 9.2 | 10.80 | 7.2 |
| | 24.0 | 19.0 | 15.0 | 14.0 | 17.5 | 23.0 | |

1157.7

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| 3.67 | 1.4 | 5.0 | 3.6 | 3.1 | 3.3 | 4.6 | 1.4 |
| | 24.0 | 18.5 | 13.5 | 15.5 | 19.0 | 25.0 | |

1152.9

| | | | | | | | | |
|------|------|------|------|------|------|------|------|-----|
| 8.79 | 3.9 | 5.9 | 7.2 | 8.1 | 7.9 | 7.6 | 9.0 | 5.2 |
| | 27.0 | 22.5 | 18.0 | 15.5 | 15.5 | 18.5 | 25.0 | |

1146.1

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| 4.18 | 1.4 | 5.8 | 4.4 | 4.1 | 3.9 | 5.3 | 1.7 |
| | 24.0 | 17.5 | 14.5 | 15.5 | 18.5 | 23.0 | |

1141.7

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| 8.68 | 9.0 | 10.4 | 8.5 | 8.5 | 8.7 | 10.5 | 9.3 |
| | 18.0 | 16.0 | 11.0 | 15.5 | 19.5 | 21.5 | |

1140.0

| | | | | | | | |
|-------|------|------|-------|-------|------|------|------|
| 10.18 | 11.1 | 12.1 | 10.50 | 10.20 | 10.5 | 12.6 | 11.9 |
| | 19.5 | 18.0 | 14.5 | 14.0 | 18.0 | 19.0 | |

1139.5

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| 3.41 | 3.4 | 5.5 | 4.0 | 3.7 | 4.3 | 6.2 | 5.7 |
| | 22.5 | 18.0 | 17.5 | 17.0 | 18.0 | 20.0 | |

S.W. Root, 48" Locust

1143.27

74+50

1139.10

74

1138.00

73

1134.60

T.P.

3.10

1135.44

10.93

1132.34

72

1131.00

71

1127.40

70

1123.80

B.M.

7.00

1128.44

1128.42 Rec.

45

1139.2

4.17 $\frac{2.3}{22.5}$ $\frac{5.3}{17.5}$ $\frac{4.0}{14.0}$ $\frac{4.1}{14.0}$ $\frac{4.5}{17.5}$ $\frac{6.1}{17.5}$ $\frac{3.5}{22.0}$

1137.8

5.27 $\frac{4.0}{21.0}$ $\frac{6.6}{16.5}$ $\frac{5.7}{14.0}$ $\frac{5.5}{14.5}$ $\frac{5.9}{14.5}$ $\frac{7.1}{18.0}$ $\frac{4.6}{22.0}$

1134.4

8.67 $\frac{7.3}{21.0}$ $\frac{10.1}{18.0}$ $\frac{9.1}{15.0}$ $\frac{8.9}{14.5}$ $\frac{9.0}{14.5}$ $\frac{10.2}{18.0}$ $\frac{8.3}{22.0}$

1131.5

4.44 $\frac{1.8}{22.0}$ $\frac{5.2}{17.5}$ $\frac{4.0}{14.0}$ $\frac{3.9}{15.0}$ $\frac{3.8}{15.0}$ $\frac{4.9}{18.5}$ $\frac{2.6}{23.0}$

1127.9

8.04 $\frac{6.4}{23.5}$ $\frac{9.3}{18.0}$ $\frac{7.7}{14.5}$ $\frac{7.5}{14.0}$ $\frac{7.5}{14.0}$ $\frac{8.9}{18.5}$ $\frac{6.0}{22.5}$

1124.1

11.64 $\frac{10.0}{21.5}$ $\frac{13.1}{17.5}$ $\frac{11.5}{13.5}$ $\frac{11.3}{14.5}$ $\frac{11.6}{14.5}$ $\frac{12.8}{18.0}$ $\frac{9.6}{22.0}$

S.W. root, 20" Pine 50Lt, sta. 70+50

B.M. 0.38 1128.80 1128.42

69 1120.20

68 1116.60

2.20 1118.16 12.84 1115.94

67 1113.15

66 1110.75

65 1109.55

64 1109.54

63 1110.50

11.61 1123.90 5.87 1112.29

62 1112.26

61 1118.00

Sept. 16, 1930

rainy 75°

S.W. root, 20" pipe 50' Lt. Sta. 70+50

8.60 $\frac{6.40}{13.5}$ $\frac{10.1}{17.5}$ $\frac{8.6}{14.0}$ $\frac{8.4}{15.0}$ $\frac{8.5}{18.5}$ $\frac{9.6}{22.0}$ $\frac{7.4}{22.0}$

12.20 $\frac{8.1}{25.5}$ $\frac{13.8}{18.0}$ $\frac{12.3}{15.0}$ $\frac{12.2}{14.0}$ $\frac{12.3}{18.0}$ $\frac{13.8}{21.0}$ $\frac{12.0}{21.0}$

5.01 $\frac{3.4}{25.5}$ $\frac{6.6}{18.5}$ $\frac{4.5}{14.5}$ $\frac{4.5}{15.0}$ $\frac{4.8}{15.0}$ $\frac{6.4}{18.0}$ $\frac{5.2}{20.0}$

7.41 $\frac{8.1}{20.5}$ $\frac{9.1}{18.5}$ $\frac{6.9}{14.0}$ $\frac{6.7}{15.0}$ $\frac{6.6}{18.0}$ $\frac{8.3}{18.0}$ $\frac{+1.0}{29.0}$

9.61 $\frac{10.3}{20.0}$ $\frac{10.8}{18.0}$ $\frac{9.2}{14.0}$ $\frac{9.0}{14.5}$ $\frac{9.2}{18.5}$ $\frac{11.0}{18.5}$ $\frac{9.9}{20.5}$

9.62 $\frac{8.5}{14.0}$ $\frac{8.8}{14.0}$ $\frac{8.9}{14.0}$

7.66 $\frac{10.2}{18.0}$ $\frac{8.7}{12.5}$ $\frac{7.9}{15.0}$ $\frac{8.3}{15.0}$ $\frac{10.2}{19.5}$ $\frac{9.7}{20.0}$

11.64 $\frac{10.2}{21.0}$ $\frac{12.5}{18.0}$ $\frac{11.1}{14.0}$ $\frac{10.9}{14.0}$ $\frac{11.0}{17.0}$ $\frac{12.3}{17.0}$ $\frac{10.7}{20.0}$

5.90 $\frac{2.6}{22.0}$ $\frac{6.9}{17.0}$ $\frac{5.2}{14.0}$ $\frac{5.7}{15.0}$ $\frac{5.7}{18.0}$ $\frac{6.6}{18.0}$ $\frac{2.5}{26.0}$

D. Parks
T. Snyder
R. Hassel

1123.90

11.98 1135.23 0.65 1123.25

60 1124.40

59 1130.33

B.M. 1.51 1133.72

1.51 1135.18 1133.67 record

58 1133.03

57 1132.50

6.62 1139.25 2.55 1132.63

56 1131.50

55 1131.00

54 1131.50

53 1132.50

1124.9

10.83 $\frac{7.0}{22.0} \frac{11.6}{18.0} \frac{10.2}{12.0} \frac{10.3}{15.5} \frac{10.4}{19.0} \frac{11.4}{28.0} \frac{7.0}{28.0}$

1130.8

4.90 $\frac{3.1}{23.5} \frac{4.1}{17.5} \frac{4.3}{14.0} \frac{4.4}{15.5} \frac{4.7}{19.0} \frac{5.7}{23.5} \frac{2.2}{23.5}$

E. root 30" pine

1132.7

2.15 $\frac{2.7}{20.0} \frac{4.3}{18.5} \frac{2.8}{15.0} \frac{2.5}{15.5} \frac{2.9}{19.0} \frac{4.2}{21.5} \frac{2.6}{21.5}$

1132.8

2.68 $\frac{1.9}{21.5} \frac{3.7}{19.5} \frac{2.3}{15.5} \frac{2.4}{15.0} \frac{3.0}{19.0} \frac{4.2}{19.0} \frac{2.4}{21.0}$

1131.5

7.75 $\frac{7.0}{21.0} \frac{9.4}{18.0} \frac{7.9}{15.5} \frac{7.8}{15.0} \frac{8.1}{15.0} \frac{9.6}{18.5} \frac{8.0}{20.0}$

1131.1

8.25 $\frac{8.7}{20.0} \frac{10.2}{18.5} \frac{8.2}{14.5} \frac{8.2}{15.0} \frac{8.8}{15.0} \frac{10.8}{18.5} \frac{9.6}{20.0}$

1131.5

7.75 $\frac{8.3}{21.0} \frac{10.0}{18.0} \frac{8.1}{14.5} \frac{7.8}{15.0} \frac{8.4}{15.0} \frac{10.4}{18.0} \frac{9.5}{20.0}$

1132.2

6.75 $\frac{7.7}{21.0} \frac{9.3}{19.0} \frac{7.2}{15.5} \frac{7.1}{14.0} \frac{7.0}{14.0} \frac{9.1}{18.0} \frac{8.0}{19.0}$

1139.25

52

1133.50

51

1135.25

50

1137.75

12.54 1151.61 0.18 1139.07

49

1140.25

48

1144.75

11.88 1162.00 1.49 1150.12

47

1151.25

46

1157.75

9.67 1171.05 0.62 1161.38

45

1163.70

B.M.

1.42 1169.63

1.87 1171.51 1169.64 record

48

1193.5

5,70

| | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|
| <u>6.5</u> | <u>8.3</u> | <u>6.1</u> | <u>5.8</u> | <u>6.0</u> | <u>8.4</u> | <u>6.7</u> |
| 20.0 | 18.0 | 14.5 | 15.0 | 15.0 | 19.0 | 21.0 |

1135.2

4,00

| | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|
| <u>4.6</u> | <u>6.2</u> | <u>4.6</u> | <u>4.1</u> | <u>4.4</u> | <u>6.9</u> | <u>4.9</u> |
| 20.0 | 18.0 | 15.0 | 15.0 | 15.0 | 19.0 | 21.0 |

1137.6

1,50

| | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|
| <u>2.4</u> | <u>3.8</u> | <u>2.3</u> | <u>1.7</u> | <u>2.2</u> | <u>3.9</u> | <u>1.6</u> |
| 20.5 | 18.5 | 15.0 | 15.0 | 15.0 | 19.0 | 21.0 |

1140.7

1,1,36

| | | | | | | |
|------------|-------------|-------------|-------------|-------------|-------------|-------------|
| <u>9.8</u> | <u>12.2</u> | <u>10.9</u> | <u>10.9</u> | <u>11.2</u> | <u>12.8</u> | <u>10.4</u> |
| 22.0 | 18.0 | 15.0 | 15.0 | 15.0 | 18.0 | 22.0 |

1144.7

6,86

| | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|
| <u>5.1</u> | <u>8.2</u> | <u>6.8</u> | <u>6.9</u> | <u>6.9</u> | <u>8.4</u> | <u>5.3</u> |
| 22.0 | 18.0 | 15.0 | 15.0 | 14.5 | 18.0 | 21.0 |

1151.2

10,75

| | | | | | | |
|------------|-------------|-------------|-------------|-------------|-------------|-------------|
| <u>9.7</u> | <u>12.6</u> | <u>10.8</u> | <u>10.8</u> | <u>11.0</u> | <u>12.9</u> | <u>10.1</u> |
| 22.0 | 18.0 | 15.0 | 15.0 | 14.5 | 17.5 | 22.0 |

1158.1

4,25

| | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|
| <u>1.2</u> | <u>5.2</u> | <u>3.7</u> | <u>3.9</u> | <u>4.1</u> | <u>5.7</u> | <u>1.4</u> |
| 25.0 | 18.0 | 14.5 | 14.5 | 14.5 | 18.0 | 22.5 |

1164.2

7,35

| | | | | | | | |
|------------|------------|------------|------------|------------|------------|------------|------------|
| <u>3.3</u> | <u>5.3</u> | <u>7.9</u> | <u>6.6</u> | <u>6.9</u> | <u>7.0</u> | <u>8.3</u> | <u>4.8</u> |
| 26.0 | 21.0 | 18.0 | 18.0 | 15.0 | 19.0 | 25.0 | |

A.P. spike, S.E. side, trunk of 27" Walnut

31' Lt., Sta. 44+60

1171.51

44

1166.00

43

1164.50

42

1162.50

41

1160.50

3.47 1162.36 12.62 1158.89

40

1158.50

39

1157.11

38

1156.95

6.84 1155.52

49

5.51

$$\begin{array}{ccccccc} \underline{5.2} & \underline{4.3} & \underline{5.1} & \underline{5.4} & \underline{6.2} & \underline{7.0} & \underline{5.9} \\ 19.5 & 17.5 & 14.5 & \cancel{4} & 16.0 & 18.5 & 20.0 \end{array}$$

7.01

$$\begin{array}{ccccccc} \underline{6.0} & \underline{8.1} & \underline{4.6} & \underline{4.7} & \underline{7.1} & \underline{8.5} & \underline{5.8} \\ 21.5 & 17.5 & 14.5 & \cancel{4} & 15.0 & 18.5 & 23.5 \end{array}$$

9.01

$$\begin{array}{ccccccc} \underline{8.7} & \underline{10.7} & \underline{8.8} & \underline{8.6} & \underline{9.0} & \underline{10.3} & \underline{7.5} \\ 22.0 & 18.0 & 15.0 & \cancel{4} & 15.5 & 18.5 & 23.0 \end{array}$$

11.01

$$\begin{array}{ccccccc} \underline{10.3} & \underline{12.6} & \underline{10.9} & \underline{10.6} & \underline{11.1} & \underline{12.4} & \underline{9.1} \\ 22.5 & 18.0 & 14.5 & \cancel{4} & 15.0 & 18.0 & 22.0 \end{array}$$

3.86

$$\begin{array}{ccccccc} \underline{2.4} & \underline{5.0} & \underline{3.5} & \underline{3.5} & \underline{3.5} & \underline{4.8} & \underline{1.8} \\ 22.5 & 18.0 & 14.5 & \cancel{4} & 14.5 & 17.5 & 23.0 \end{array}$$

5.26

$$\begin{array}{ccccccc} \underline{5.8} & \underline{7.3} & \underline{5.1} & \underline{5.0} & \underline{5.2} & \underline{7.0} & \underline{13.6} \\ 20.5 & 17.0 & 13.0 & \cancel{4} & 14.5 & 18.0 & 22.5 \end{array}$$

5.41

$$\begin{array}{ccccccc} \underline{6.9} & \underline{8.0} & \underline{5.9} & \underline{5.8} & \underline{6.2} & \underline{7.8} & \underline{7.4} \\ 20.0 & 18.5 & 14.5 & \cancel{4} & 13.0 & 17.0 & 18.0 \end{array}$$

Slope hub Lt. Sta. 38+00

Sept, 17, 1930

D. Parks

R. Hassel

50

cloudy 70°

T. Snyder

slope hub Lt sta. 38+00

| | | | | |
|-------|-------|---------|------|---------|
| T. P. | 12.80 | 1168.32 | | 1155.52 |
| 37 | | | | 1158.10 |
| | 9.61 | 1174.73 | 3.20 | 1165.12 |
| 34 | | | | 1163.40 |
| 35 | | | | 1167.90 |
| 34 | | | | 1169.40 |
| 33 | | | | 1169.92 |
| 32 | | | | 1170.96 |
| | 11.57 | 1183.89 | 2.41 | 1172.32 |
| 31 | | | | 1172.37 |
| 30 | | | | 1176.00 |
| 29 | | | | 1178.38 |

| | | | | | |
|-------|------|------|------|------|------|
| | 10.0 | 11.5 | 9.9 | 10.3 | 12.6 |
| 10.22 | 21.0 | 18.0 | 15.0 | 13.5 | 18.0 |

| | | | | | | | |
|-------|------|------|------|------|------|------|-----|
| | 4.7 | 11.7 | 10.3 | 10.3 | 10.9 | 11.9 | 8.7 |
| 11.33 | 29.0 | 18.0 | 15.0 | 14.0 | 17.0 | 23.5 | |

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| | 2.0 | 7.5 | 6.5 | 6.5 | 6.9 | 8.3 | 6.7 |
| 6.83 | 26.0 | 18.0 | 15.0 | 14.0 | 18.0 | 21.0 | |

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| | 1.2 | 6.5 | 5.2 | 5.1 | 5.8 | 7.3 | 6.1 |
| 5.33 | 25.0 | 18.0 | 14.5 | 13.5 | 18.0 | 17.5 | |

| | | | | | | | |
|------|------|------|------|------|------|-----|--|
| | 3.1 | 6.8 | 4.9 | 4.9 | 5.2 | 7.4 | |
| 4.81 | 22.0 | 18.0 | 13.0 | 15.0 | 19.0 | | |

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| | 2.0 | 5.0 | 3.6 | 3.7 | 4.3 | 5.7 | 4.7 |
| 3.77 | 21.0 | 17.5 | 14.5 | 15.0 | 17.5 | 18.5 | |

| | | | | | | | |
|-------|------|------|------|------|------|------|------|
| | 11.6 | 12.9 | 11.3 | 11.2 | 11.9 | 13.4 | 13.1 |
| 11.52 | 20.0 | 18.0 | 14.0 | 14.0 | 17.0 | 18.5 | |

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| | 3.8 | 8.2 | 7.1 | 7.7 | 8.3 | 9.2 | 7.9 |
| 7.89 | 23.0 | 18.0 | 14.0 | 15.5 | 18.0 | 20.0 | |

| | | | | | | | |
|------|------|------|------|------|------|------|-----|
| | 2.1 | 5.5 | 4.4 | 4.9 | 5.6 | 6.8 | 4.9 |
| 5.51 | 21.0 | 18.0 | 14.0 | 15.5 | 19.0 | 21.5 | |

1183.89

B.M

0.79 1183.10

0.79 1183.84

1183.05 record

28

1177.50

27

1175.00

26

1172.50

2.12 1173.02 12.94 1170.90

25

1170.00

24

1166.80

23

1163.60

22

1162.00

21

1162.00

1.61 1164.09 10.54 1162.48

20

1162.00

spike south root 20" Maple

^{1177.6}

$$\begin{array}{ccccccc} 3.8 & 4.9 & 5.9 & 6.2 & 6.3 & 7.7 & 5.8 \\ 6.34 & 21.0 & 18.0 & 14.5 & \cancel{4} & 15.0 & 18.0 & 20.0 \end{array}$$
^{1175.0}

$$\begin{array}{ccccccc} 5.4 & 9.2 & 8.5 & 8.8 & 9.5 & 10.7 & 8.7 \\ 8.84 & 24.0 & 18.0 & 15.0 & \cancel{4} & 15.0 & 18.0 & 20.0 \end{array}$$
^{1172.3}

$$\begin{array}{ccccccc} 11.3 & 12.9 & 11.4 & 11.5 & 11.8 & 14.1 & 13.0 \\ 11.34 & 20.0 & 18.0 & 15.0 & \cancel{4} & 15.0 & 18.0 & 21.0 \end{array}$$
^{1170.1}

$$\begin{array}{ccccccc} 1.4 & 4.2 & 2.8 & 2.9 & 3.3 & 4.9 & 7.8 \\ 3.02 & 23.0 & 18.0 & 14.0 & \cancel{4} & 14.5 & 17.5 & 18.0 \end{array}$$
^{1167.7}

$$\begin{array}{ccccccc} 1.7 & 6.4 & 5.1 & 5.3 & 5.4 & 7.4 & 4.8 \\ 6.22 & 26.0 & 19.0 & 15.5 & \cancel{4} & 14.0 & 18.0 & 21.5 \end{array}$$
^{1164.0}

$$\begin{array}{ccccccc} 5.9 & 9.9 & 8.9 & 9.0 & 9.6 & 11.3 & 8.1 \\ 9.42 & 24.0 & 18.5 & 15.5 & \cancel{4} & 15.0 & 18.5 & 21.5 \end{array}$$
^{1162.1}

$$\begin{array}{ccccccc} 13.7 & 11.1 & 10.9 & & 11.4 & 14.6 & \\ 11.02 & 22.0 & 15.0 & \cancel{4} & 16.0 & 20.5 & \end{array}$$
^{1162.6}

$$\begin{array}{ccccccc} 7.2 & 11.2 & 10.2 & 10.4 & 10.6 & 12.3 & 9.3 \\ 11.02 & 22.5 & 18.0 & 14.5 & \cancel{4} & 14.0 & 18.0 & 21.0 \end{array}$$
^{1162.4}

$$\begin{array}{ccccccc} +0.1 & 2.6 & 1.7 & 1.7 & 2.1 & 3.3 & 0.9 \\ 2.09 & 23.0 & 18.0 & 15.0 & \cancel{4} & 14.0 & 18.0 & 20.5 \end{array}$$

1164.09

19

1161.20

18

1159.60

17

1157.90

B.M.

7.40 1156.69

3.66 1160.21

1156.55 record

16

1155.60

15

1153.10

14

1149.90

1.34 1148.86 12.69 1147.52

13

1146.00

12

1141.60

11

1136.50

52

1161.1

| | | | | | | |
|------|------|------|-----|------|------|------|
| 1.6 | 4.1 | 2.8 | 3.0 | 3.9 | 5.2 | 3.3 |
| 23.0 | 19.0 | 16.0 | £ | 17.5 | 18.0 | 20.5 |

2.89

1159.7

| | | | | | | |
|------|------|------|-----|------|------|------|
| 4.0 | 5.7 | 4.4 | 7.7 | 5.0 | 6.5 | 4.6 |
| 20.0 | 18.0 | 14.5 | £ | 14.5 | 18.5 | 21.0 |

4.49

1158.7

| | | | | | | |
|------|------|------|-----|------|------|------|
| 3.0 | 5.5 | 5.0 | 5.4 | 5.9 | 7.2 | 5.4 |
| 20.5 | 17.5 | 14.0 | £ | 15.5 | 19.0 | 21.0 |

6.19

Bent spike N.W. root 24" Maple 28.5 ft, 16+14

1155.5

| | | | | | | |
|------|------|------|-----|------|------|------|
| 2.5 | 4.9 | 4.2 | 4.7 | 5.3 | 7.1 | 4.4 |
| 21.5 | 18.5 | 16.5 | £ | 14.5 | 17.0 | 21.5 |

4.61

1152.8

| | | | | | | |
|------|------|------|-----|------|------|------|
| 5.9 | 7.7 | 7.3 | 7.4 | 8.2 | 9.5 | 8.9 |
| 21.5 | 18.5 | 16.5 | £ | 15.0 | 18.5 | 19.5 |

7.11

1150.1

| | | | | | | |
|------|------|------|------|------|------|------|
| 7.8 | 10.2 | 9.5 | 10.1 | 10.5 | 11.5 | 9.2 |
| 21.0 | 18.5 | 15.0 | £ | 15.0 | 18.0 | 20.5 |

10.31

1146.1

| | | | | | | |
|------|------|------|-----|------|------|------|
| 1.0 | 4.1 | 2.9 | 2.8 | 3.2 | 4.4 | 1.7 |
| 22.0 | 17.0 | 14.0 | £ | 15.5 | 18.5 | 22.0 |

2.86

1141.5

| | | | | | | |
|------|------|------|-----|------|------|------|
| 3.7 | 8.0 | 7.1 | 7.4 | 7.9 | 9.7 | 6.4 |
| 23.0 | 18.0 | 15.0 | £ | 14.5 | 17.0 | 21.0 |

7.24

1136.5

| | | | | | | |
|------|------|------|------|------|------|------|
| 9.6 | 7.1 | 12.2 | 13.4 | 13.0 | 14.7 | 11.4 |
| 23.0 | 18.0 | 15.0 | £ | 14.5 | 17.5 | 21.0 |

12.36

1148.86

4.71 1141.03 12.54 1136.32

10 1130.50

1.63 1131.11 11.55 1129.48

9 1122.00

8 1113.57

0.01 1120.53 10.59 1120.52

8 1113.57

B.M. 4.98 1115.55

4.98 1120.48 1115.50 record

1.27 1109.46 12.29 1108.19

7 1106.30

6 1099.58

0.62 1097.46 12.62 1096.84

5 1093.10

4 1088.29

1131.1

10.53 $\frac{7.9}{24.5}$ $\frac{9.8}{18.0}$ $\frac{9.7}{15.0}$ $\frac{9.9}{14.0}$ $\frac{10.3}{17.0}$ $\frac{11.0}{17.0}$ $\frac{9.5}{19.0}$

1122.9

9.110 $\frac{0.6}{27.0}$ $\frac{8.8}{17.0}$ $\frac{8.0}{15.0}$ $\frac{8.2}{16.0}$ $\frac{8.6}{19.0}$ $\frac{10.8}{19.0}$ $\frac{7.5}{19.0}$

12.2

17.54 $\frac{12.2}{27.0}$

1113.5

4.96 $\frac{7.7}{19.0}$ $\frac{6.9}{14.0}$ $\frac{7.0}{15.0}$ $\frac{7.4}{19.0}$ $\frac{9.5}{19.0}$ $\frac{8.1}{21.0}$

Spike N.W. root 20" Maple, 30' Pt. Sta. 8+30

1106.1

3.16 $\frac{0.0}{24.0}$ $\frac{4.5}{19.0}$ $\frac{3.1}{15.0}$ $\frac{3.4}{16.0}$ $\frac{3.8}{19.0}$ $\frac{5.7}{19.0}$ $\frac{3.9}{22.0}$

1099.8

9.88 $\frac{5.5}{22.0}$ $\frac{10.8}{18.0}$ $\frac{9.3}{14.5}$ $\frac{9.7}{15.0}$ $\frac{10.2}{18.5}$ $\frac{11.8}{18.5}$ $\frac{7.2}{25.5}$

1093.8

4.36 $\frac{1.0}{22.0}$ $\frac{4.6}{19.0}$ $\frac{3.2}{15.0}$ $\frac{3.7}{15.0}$ $\frac{4.1}{18.0}$ $\frac{5.7}{18.0}$ $\frac{1.9}{24.0}$

1088.7

9.22 $\frac{7.0}{21.0}$ $\frac{9.8}{18.0}$ $\frac{8.6}{14.5}$ $\frac{8.8}{15.0}$ $\frac{9.3}{17.5}$ $\frac{10.5}{17.5}$ $\frac{8.3}{24.0}$

1097.46

0.62 1086.04 12.04 1085.42

3 1085.00

2 1082.00

1 1078.75

B.M. 10.96 1075.08

1075.05 record

1092.9

1.04 $\frac{0.5}{20.0}$ $\frac{2.5}{18.0}$ $\frac{1.3}{14.5}$ $\frac{1.2}{15.0}$ $\frac{1.4}{19.0}$ $\frac{3.2}{22.0}$ $\frac{1.6}{22.0}$

1091.7

4.04 $\frac{4.8}{20.0}$ $\frac{6.1}{18.0}$ $\frac{4.6}{14.0}$ $\frac{4.3}{14.0}$ $\frac{4.7}{18.0}$ $\frac{6.0}{20.5}$ $\frac{4.7}{20.5}$

1078.9

7.29 $\frac{6.9}{21.0}$ $\frac{9.0}{18.0}$ $\frac{7.0}{14.0}$ $\frac{7.1}{14.5}$ $\frac{7.6}{18.0}$ $\frac{8.2}{20.0}$ $\frac{7.7}{20.0}$

X-on S.E. corner South Headwall Culvert O+20

Richards
Hosford
Gundarsan

(Plot)

Taylor-May Rd

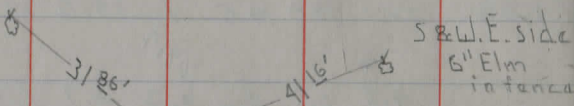
fr. Snudars Cor's Rd. to Brown's Cor's Rd.

24/7/91

Bent
s&w. E. side 12"
Ash

Sta. 17+87.00

$\Delta = 38^{\circ} 57'$ Lt



Boat Spk. Sat

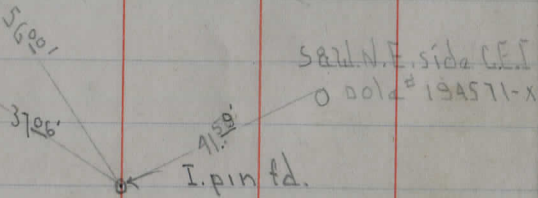
S&W. S. side
12" Ash

Spk. N. side 20" Elm

S&W. N. side Tal.
pole

Sta. 0+0

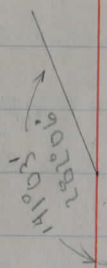
Bag. Proj.



I. pin fd.

F.B. 83

551



$\Delta = 38^{\circ} 57'$ Lt.
 $\Delta = 35^{\circ}$
 P.I. = 17+87.00
 P.C. = 17+28.23
 P.T. = 18+45.11
 Ext. = 11.11'
 $R = 186.395$

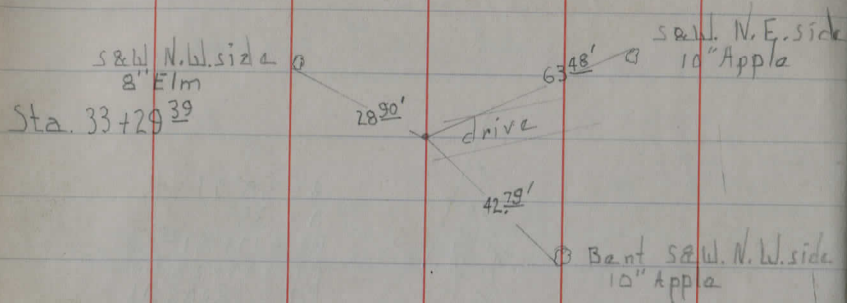
x P.L. x 17+08.5 x

Z —————

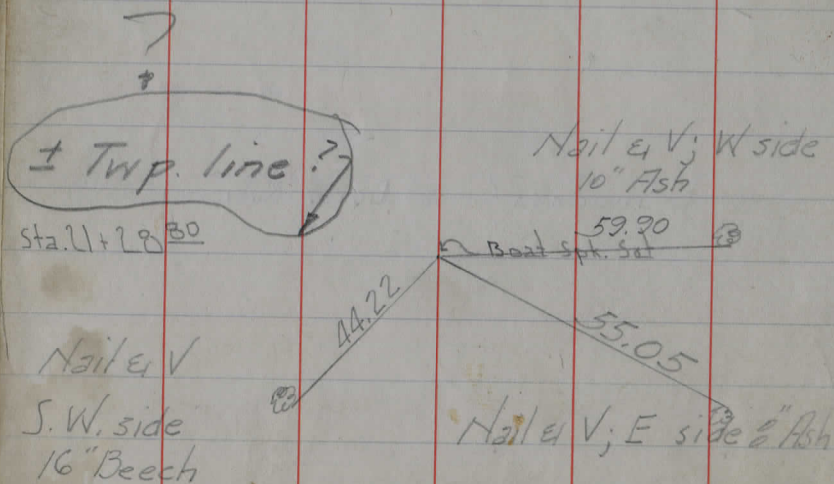
10+20 Drive

x P.L. x 10+15.5 x

Snudars Cor's Rd.



- 32+0 Spk. sat for line + Dist
- +78 Approx. Top Line
- 31+0 Spk. sat for Dist + line
- 29+0 quit Spk ok for dist. only



P.O.T. Boat spk set

PT = 23+12.74

$\Delta = 11^{\circ}05'$ Rt.

D = 3°

R = 1909.859

T = 185.30

L = 369.44

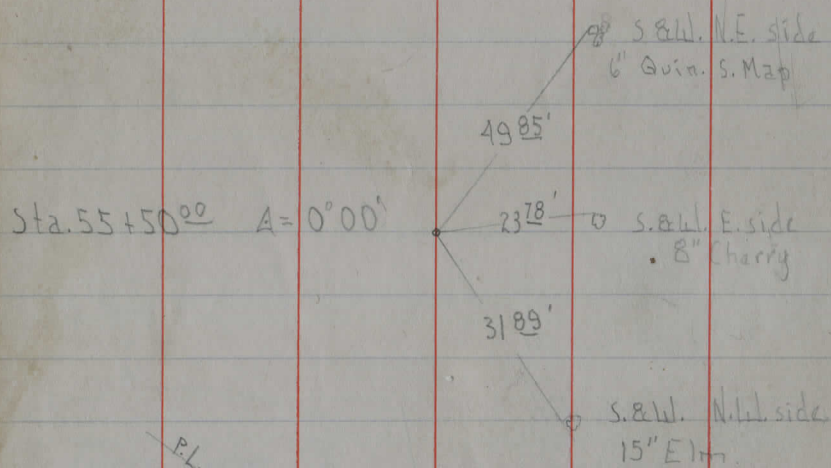
E = 8.96

168.55

337.50

PC = 19+43.50

57+9



Sta. 54+14⁰⁰

I.P. →

30'

Spk.

45+63

(for Int. see
FB 308 pg. 9)

Spk. set

1190 ft.

Spk. set

Road Quinn
Tad

P.O.T.

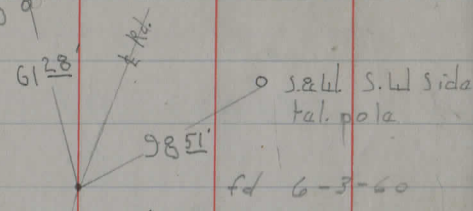
Boat Spk set
Fa 5/7/60

I.P. fd

30'

Spk set

P.T. 78+28⁵³
S&W.S side
C.E.I.# 515610



Sta. 77+23⁰⁰

P.C. = 76+13⁰⁸

s&W.S side
C.E.I. # 515611

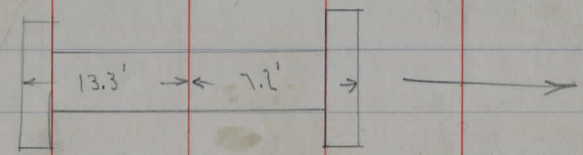
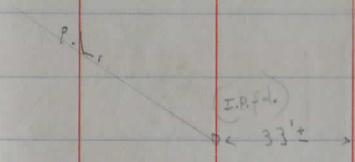
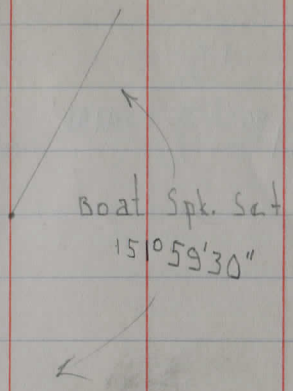
73+55^E

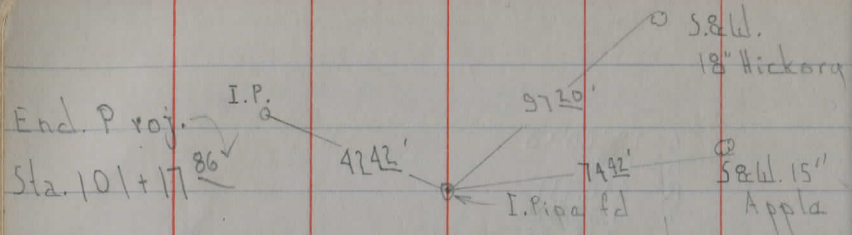
Sta 68+75^E (3.5' x 3') stone Box Fair Cond.

Sta. 67+00

← spk. set

$\Delta = 28^{\circ} 00' 30''$
 $D = 13^{\circ}$
 $R = 440.737'$
 $T = 108.92'$
 $L = 215.45'$
 $E = 13.5'$

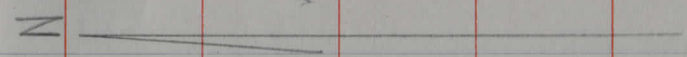
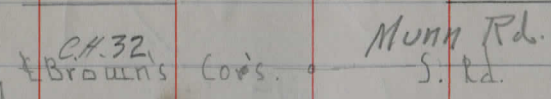




Sta. 89+0

Sph. Set

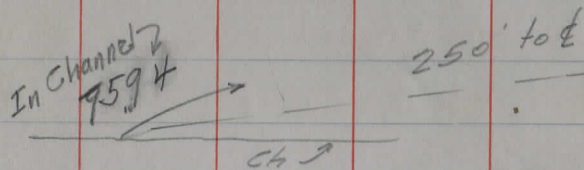
80+36



x P.L. x x

Stakes for relocation
of culvert Taylor - May Road

See levels next page



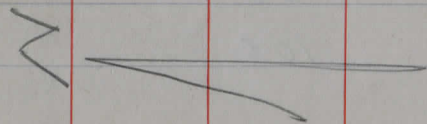
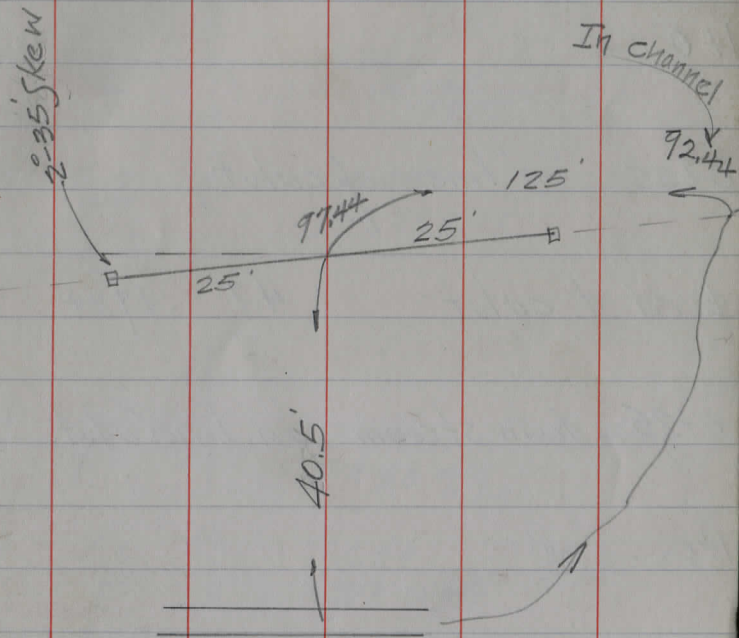
68175^S Existing 3.5 x 3' ^{deep} stone box.
= 11.5 sq ft.

Note: Increase size of new
culvert or leave old culvert
for floods

5-29-42

60

Pomeroy
Gundersen



See preceeding page

| | + | - | Grade |
|--------------------|---------------------------|------------------------------|--------|
| B.M. | 2.14 | 102.14 | 100.00 |
| Sta. 2+50 upstream | | Chan 6.2 Grade 6.74 | 95.74 |
| 2+0 | " | | 94.90 |
| 1+0 | " | | |
| 0+25 | on line of culvt | | |
| £ rd £ culvt | | 4.7 | 97.44 |
| 0+25 | down stream on line Culvt | | |
| 1+0 | " | | |
| 1+25 | " | | 92.44 |
| 2+0 | " | 10.5 | |
| 3+0 | " | 10.8 | |

Rod Spike N.W. root 12" W. Ch. 68±50
28' Rt

| | | | |
|------|------------|------------------------------|-----------|
| 7.24 | 5.3 £ | 3.74 Stk 10' off | Cut 3'-6" |
| 8.24 | 6.1 £ | 5.24 Stk 10' off | C 3'-0" |
| 8.99 | 6.0 grd | 4.49 Stk 25' off £ rd. | C 4'-6" |
| 9.49 | 6.6 grd | 5.04 Stk 25' off £ rd | C 4'-6" |
| 9.79 | 8.0 £ | 6.29 Stk 10' off | C 3'-6" |
| 9.89 | 9.7 ch | 6.39 Stk 10' off | C 3'-6" |

1.00% grade

0.4%



IRON PIPE FOUND
10-28-55

FENCE & R?

RAIL Road
Spike N.E. side
36" Maple

SPIKE S.W. side
30" Map.

SPIKE S.E. side
24" Map.

(TAYLOR
(CANFIELD

(MAY
(RD)

APPROX. 650'

STATE R/W Mon.

Center of
APPARENT DRILL HOLE
HEAD WALL

58.2

36.24

39.5

N.E. COR HEADWALL
?

PAINESVILLE - RAVENNA RD.

Munn Rd.

90-00-30

2085.65
Taylor-May

IP = 1.10 down
(9.5 N. of Painted Post)

89-52

I.P.
30"



I.P.

64-12-30

212.95
Thorp Rd.
I.P.

See Blk #145 pg 49
Taylor-May

5.8 W
12" Map

Bldg
3 Tacks
SE

100.7

8.5 W
6" pear

Auburn

5800
RD

2" I. pin
± 5' E of
¢ of
Aub. Rd.



Spk SW side
CEI 192333

90-13-30

39.19

205.08

30

426.8

90°

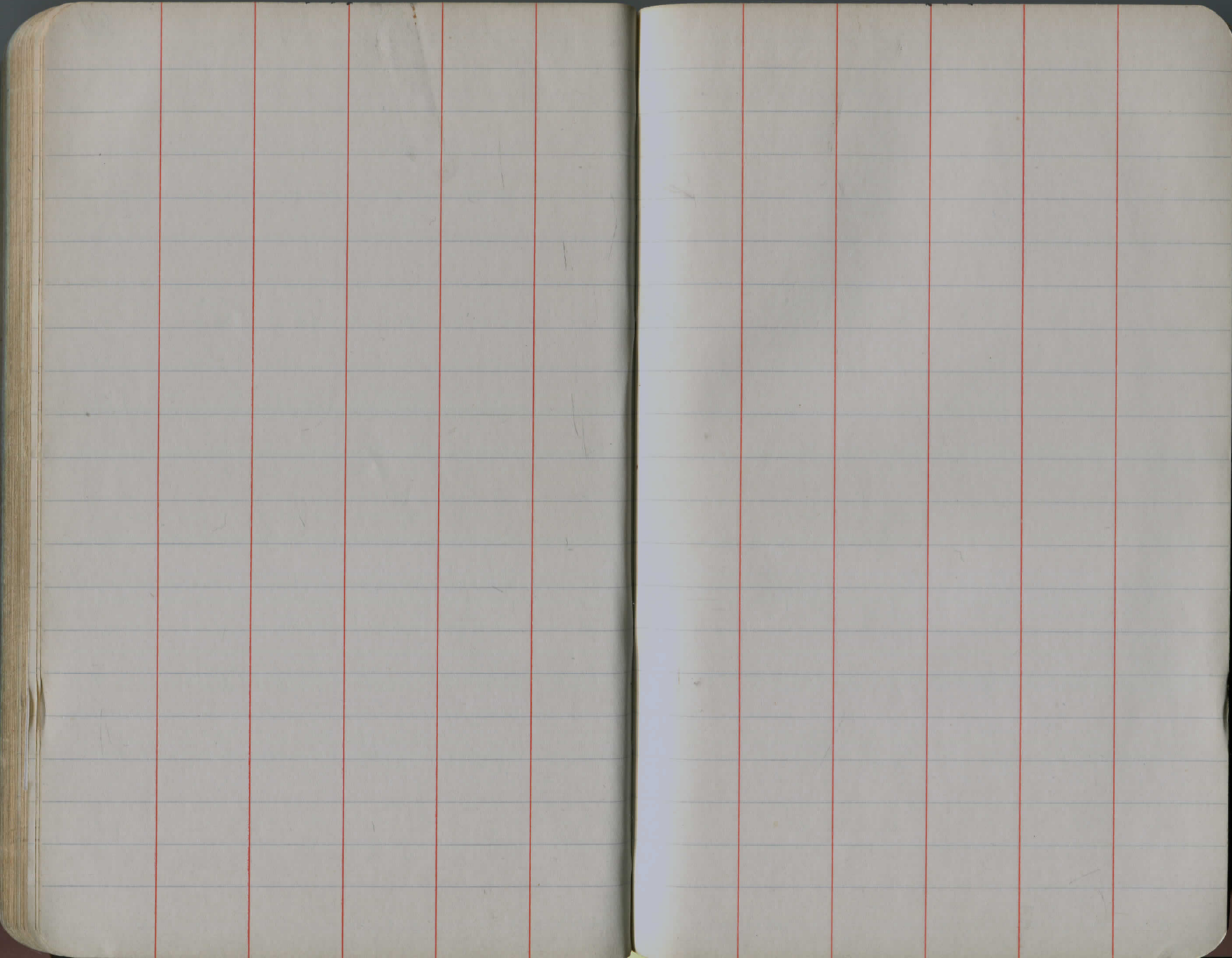
400±

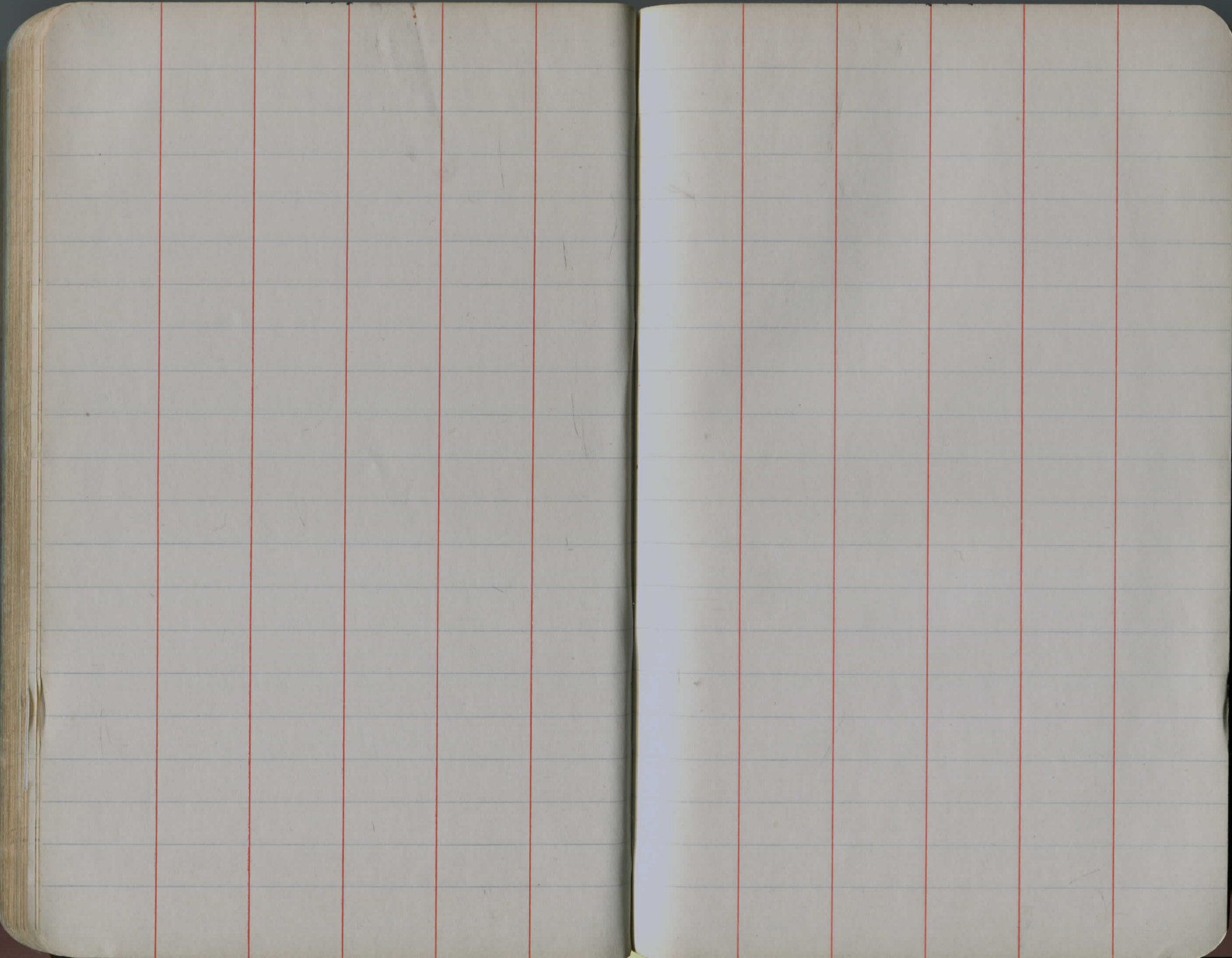
170-47

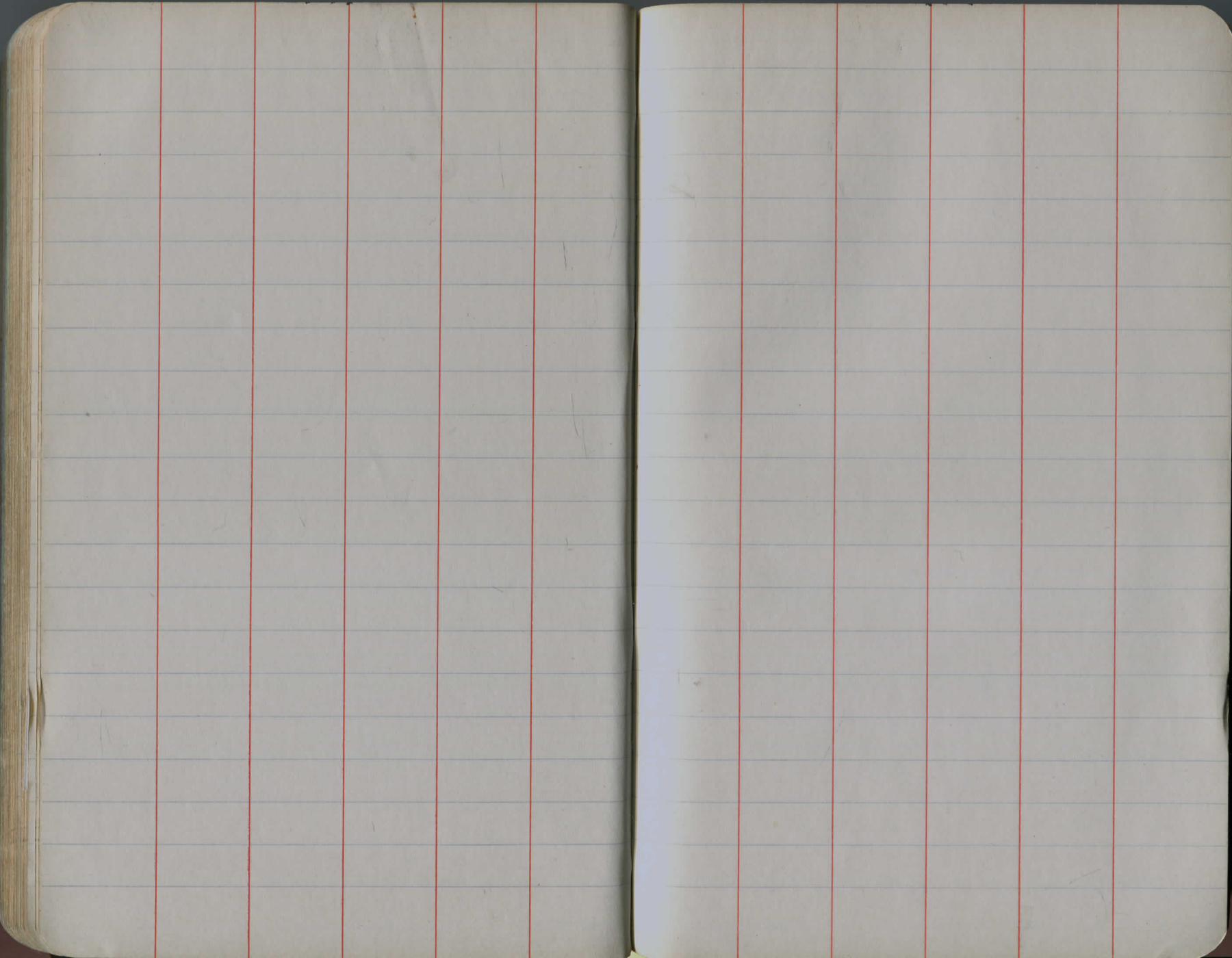
31.77

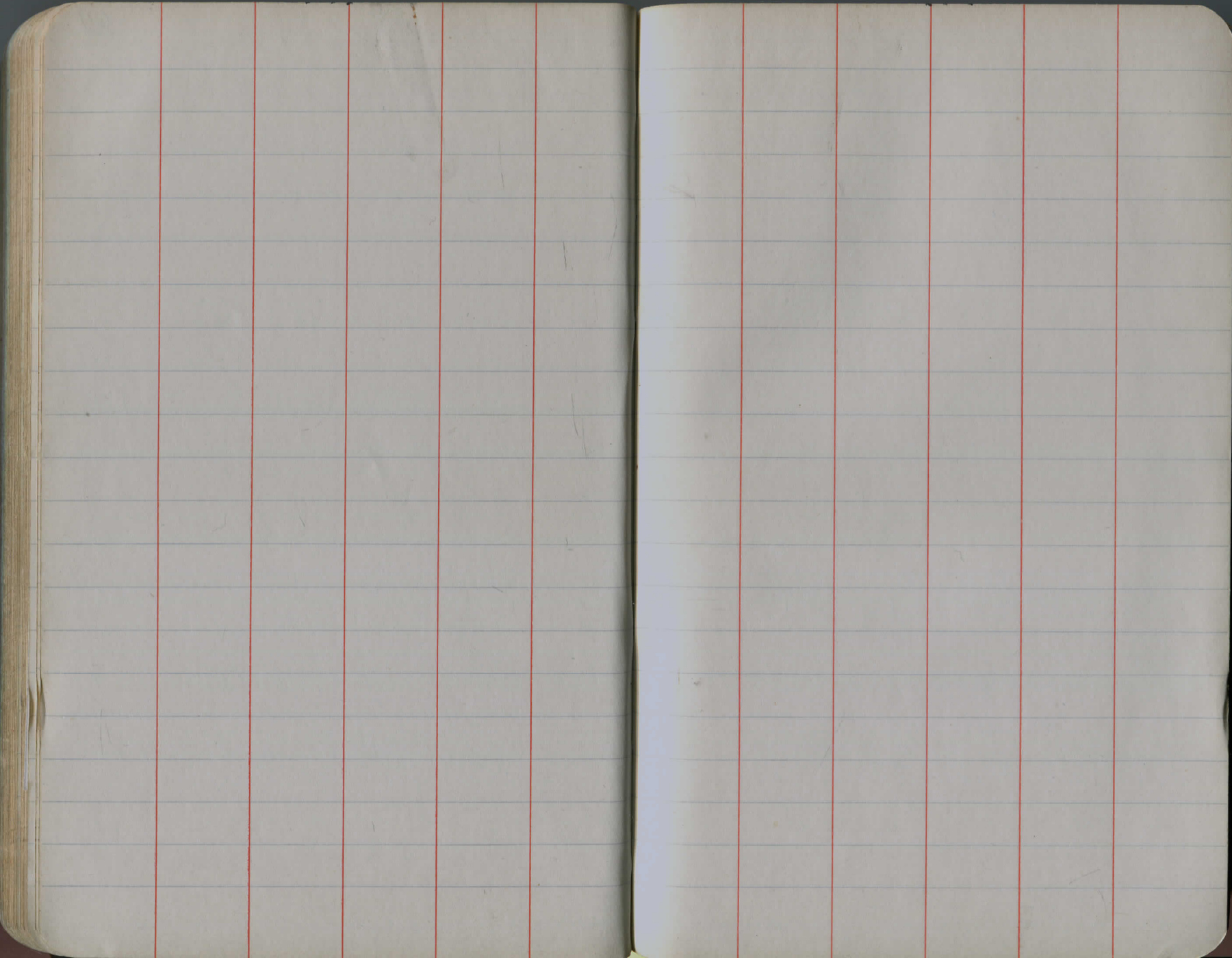
3/4" IP

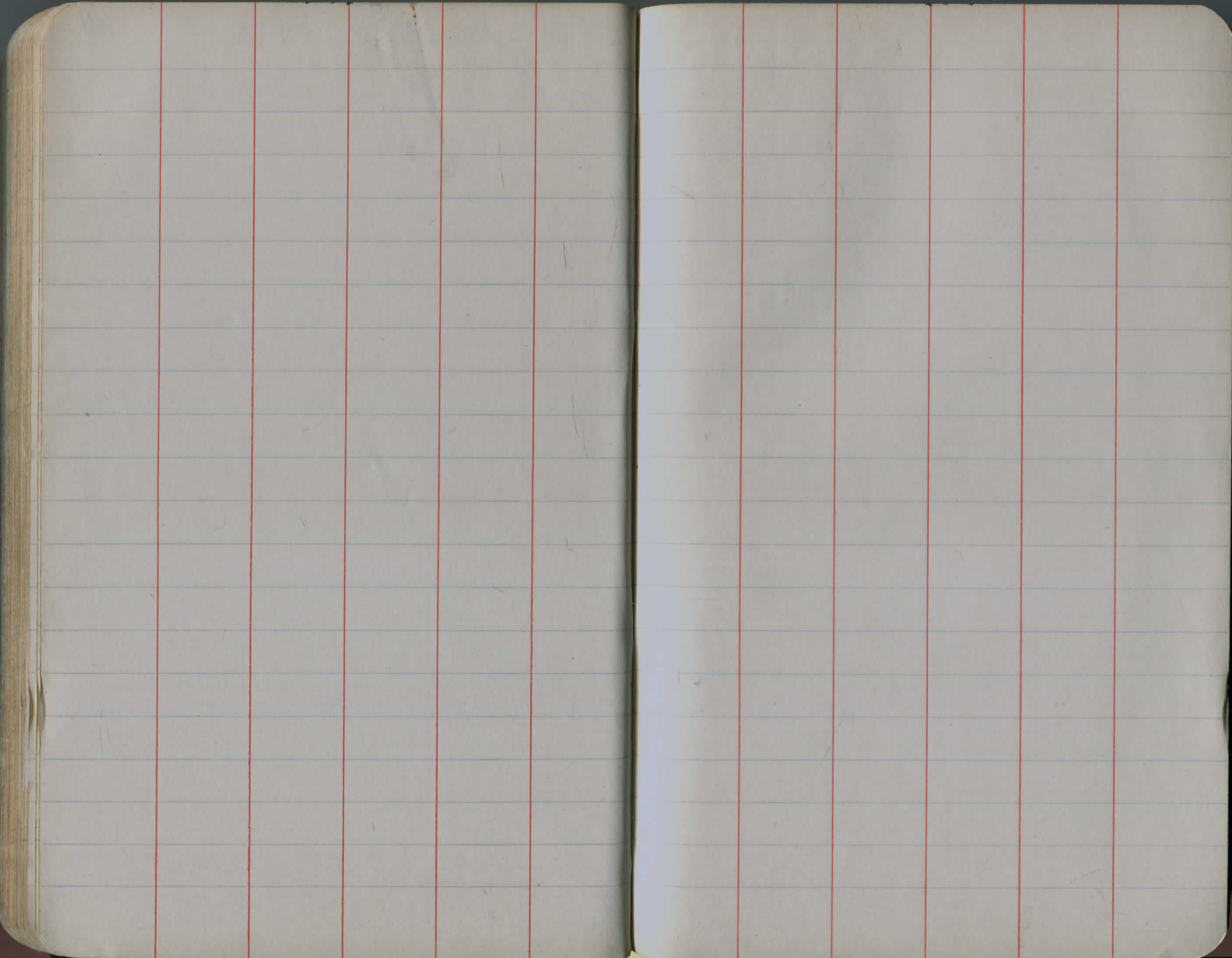
Prop. Line
I.P.

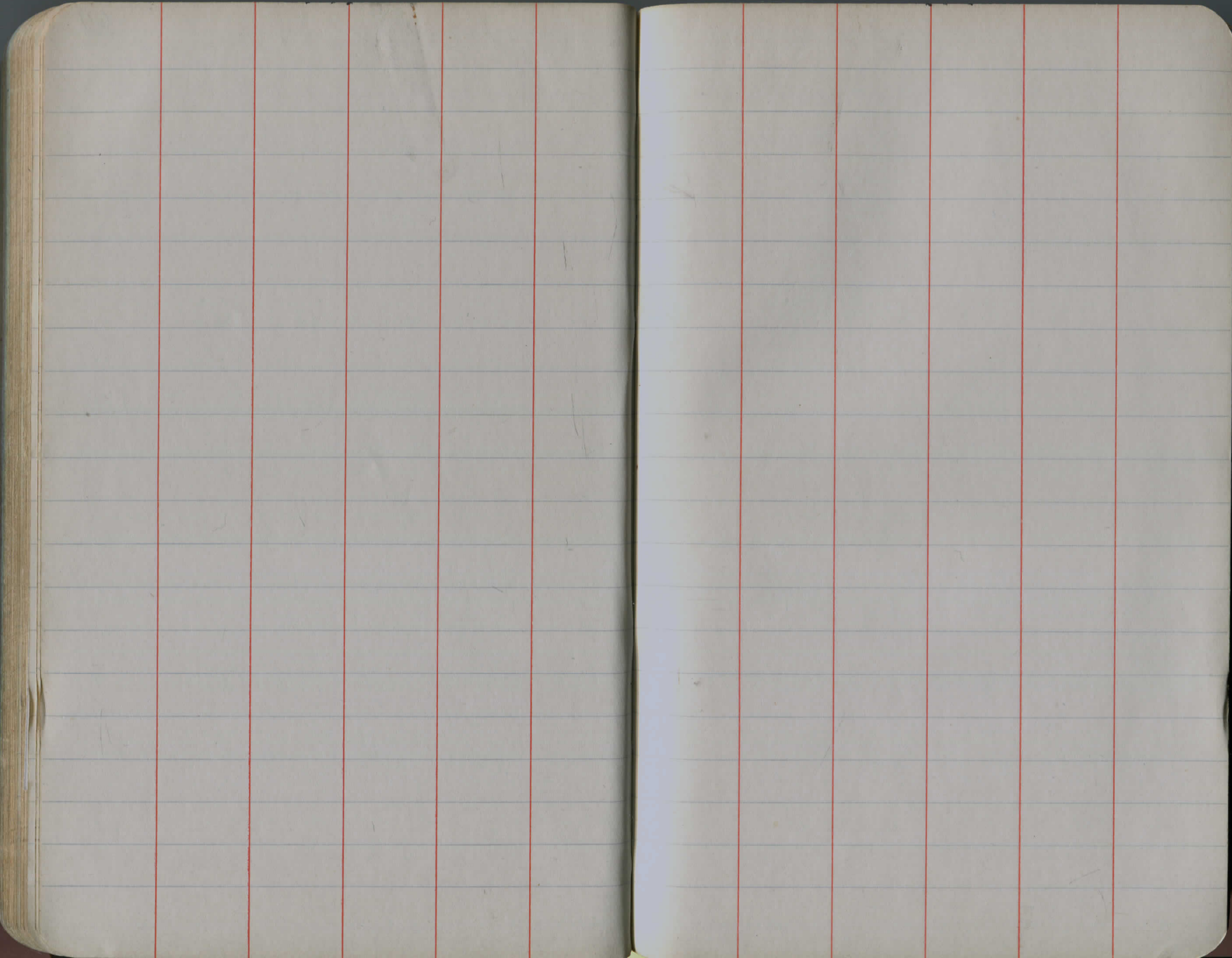


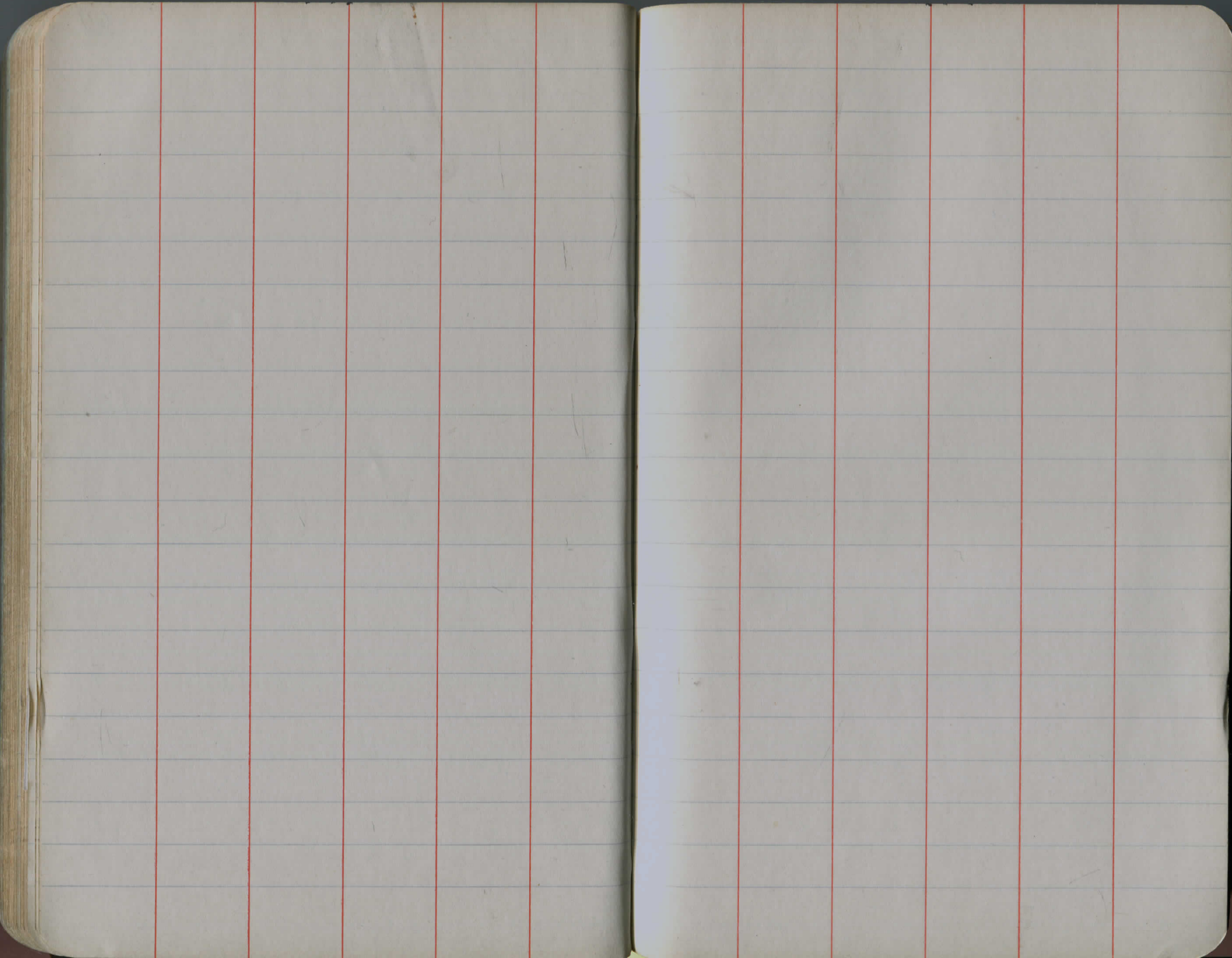


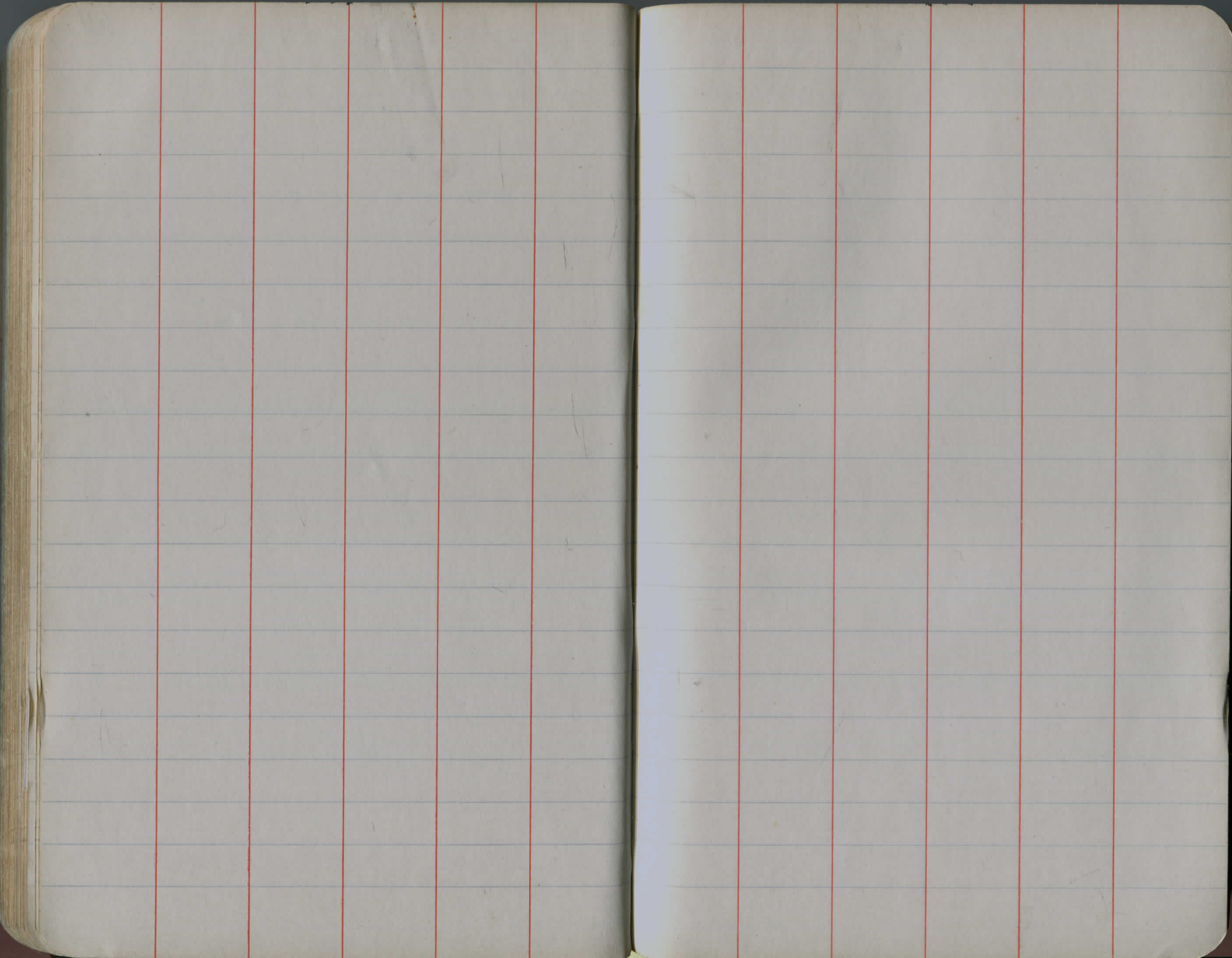


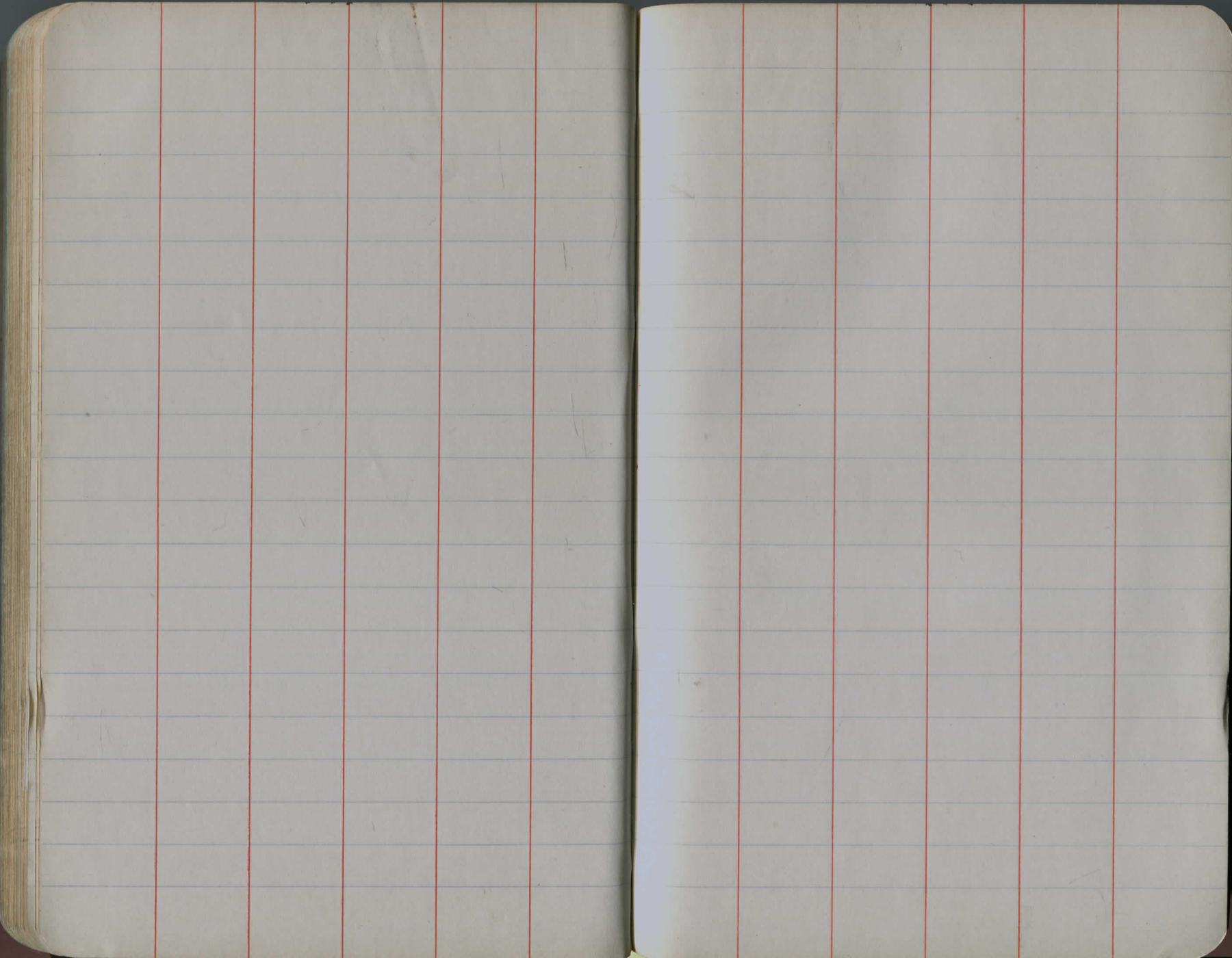


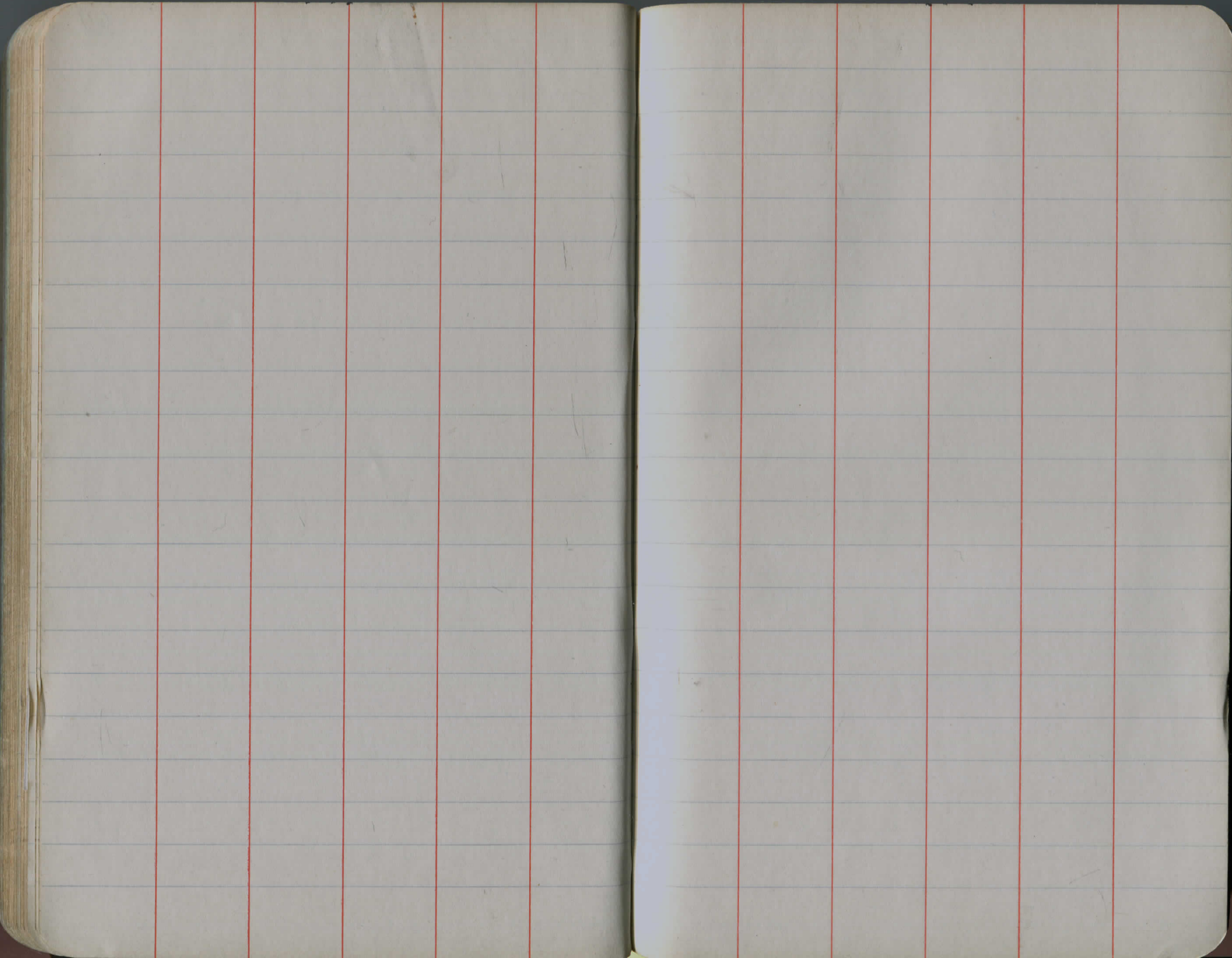


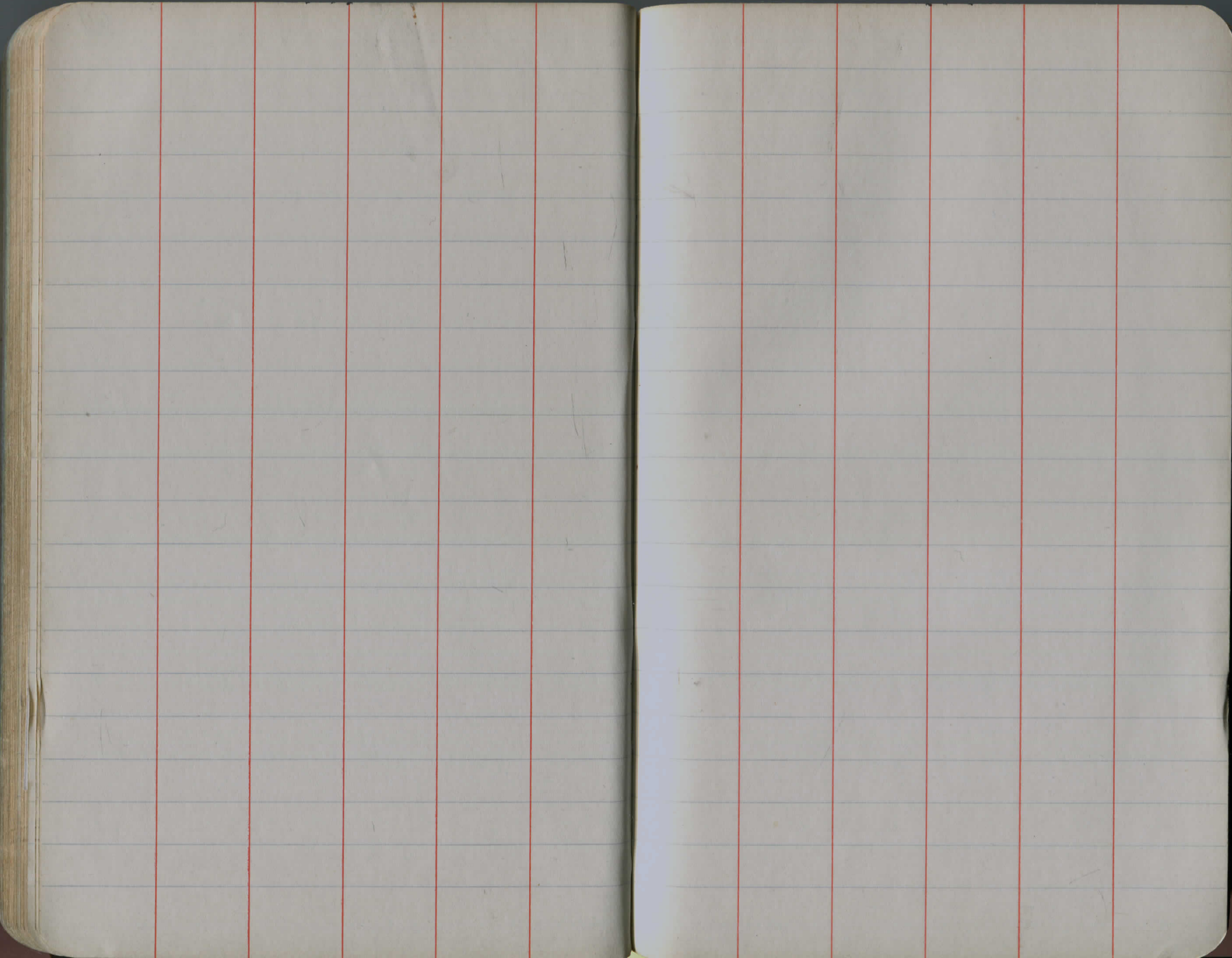


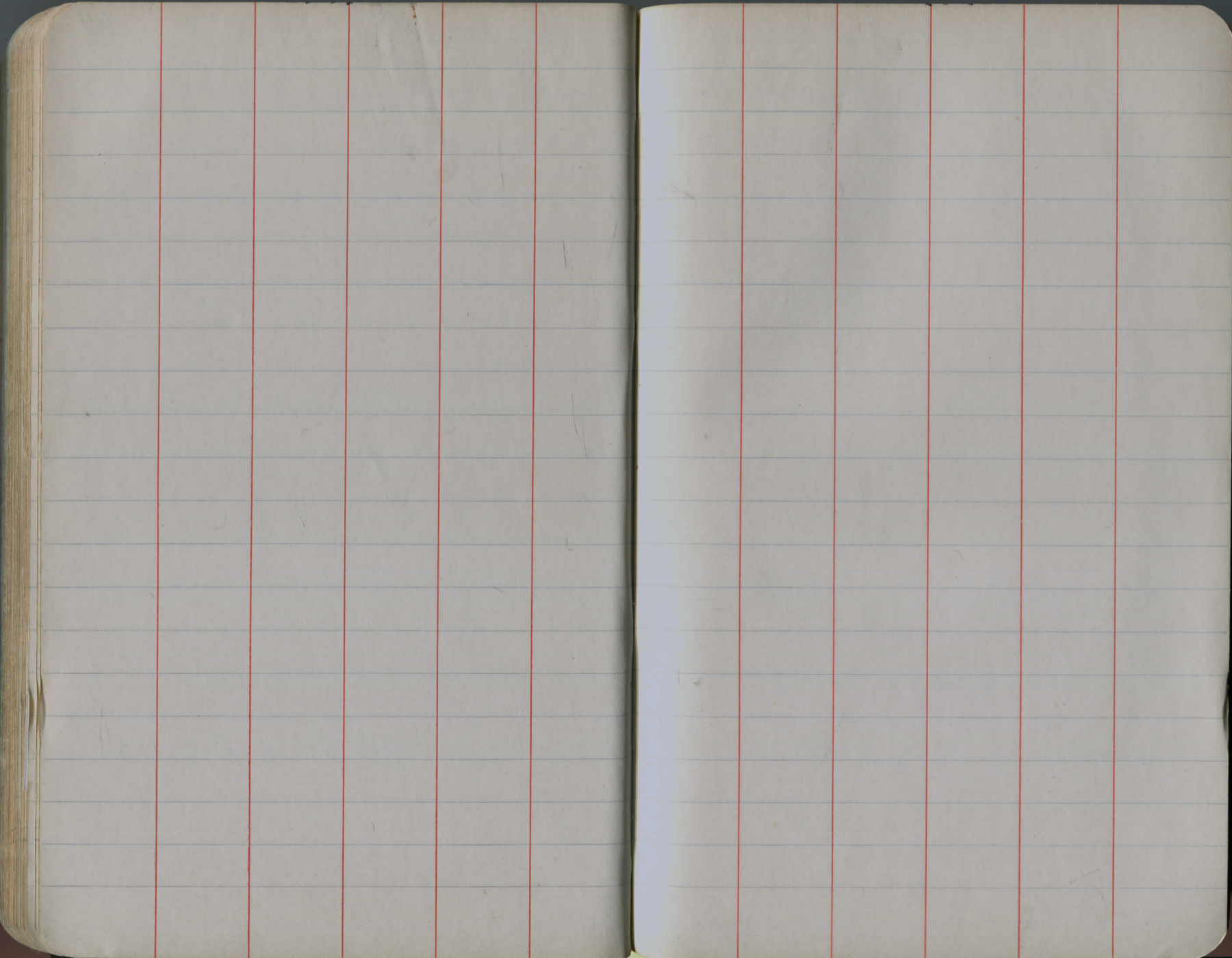


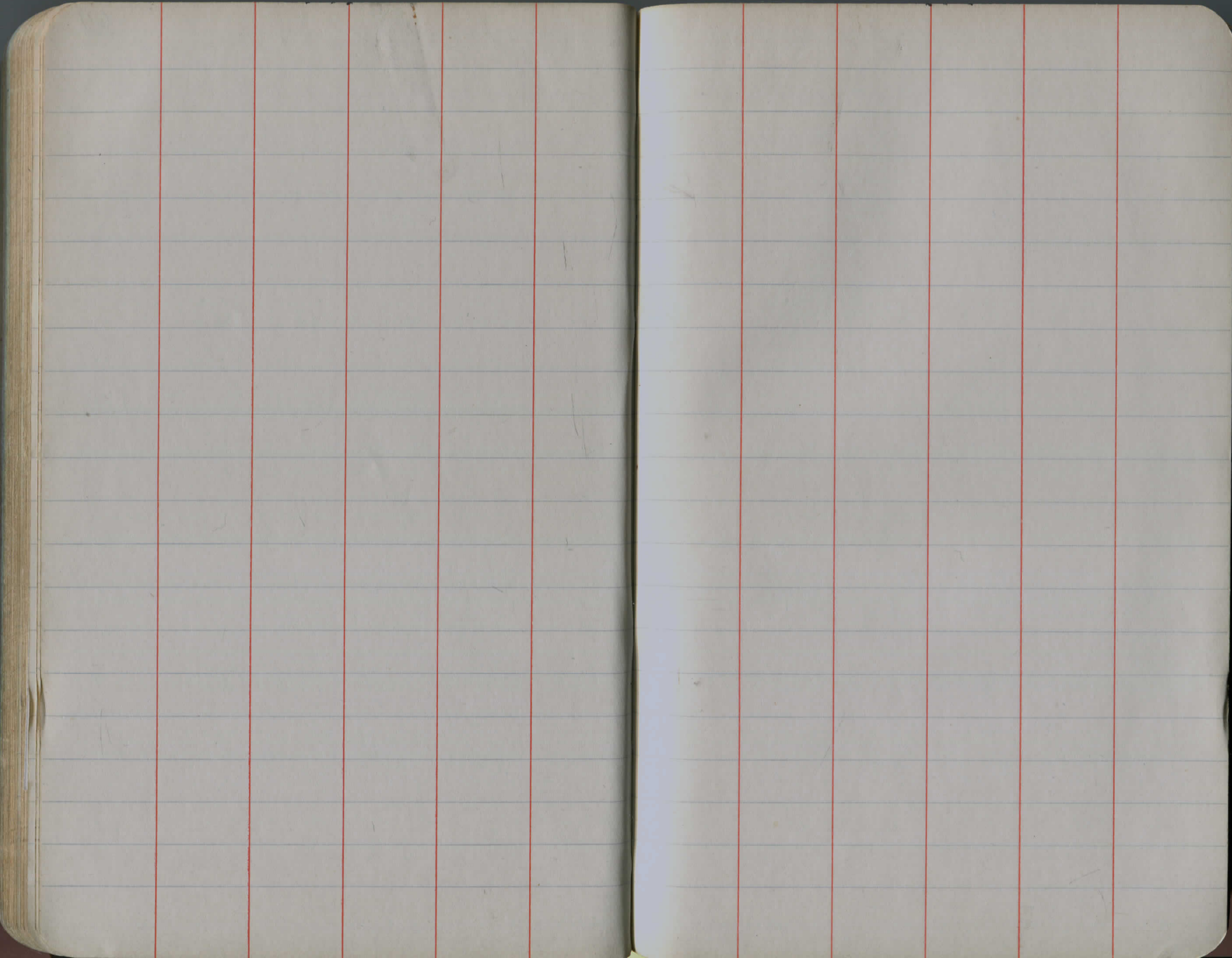


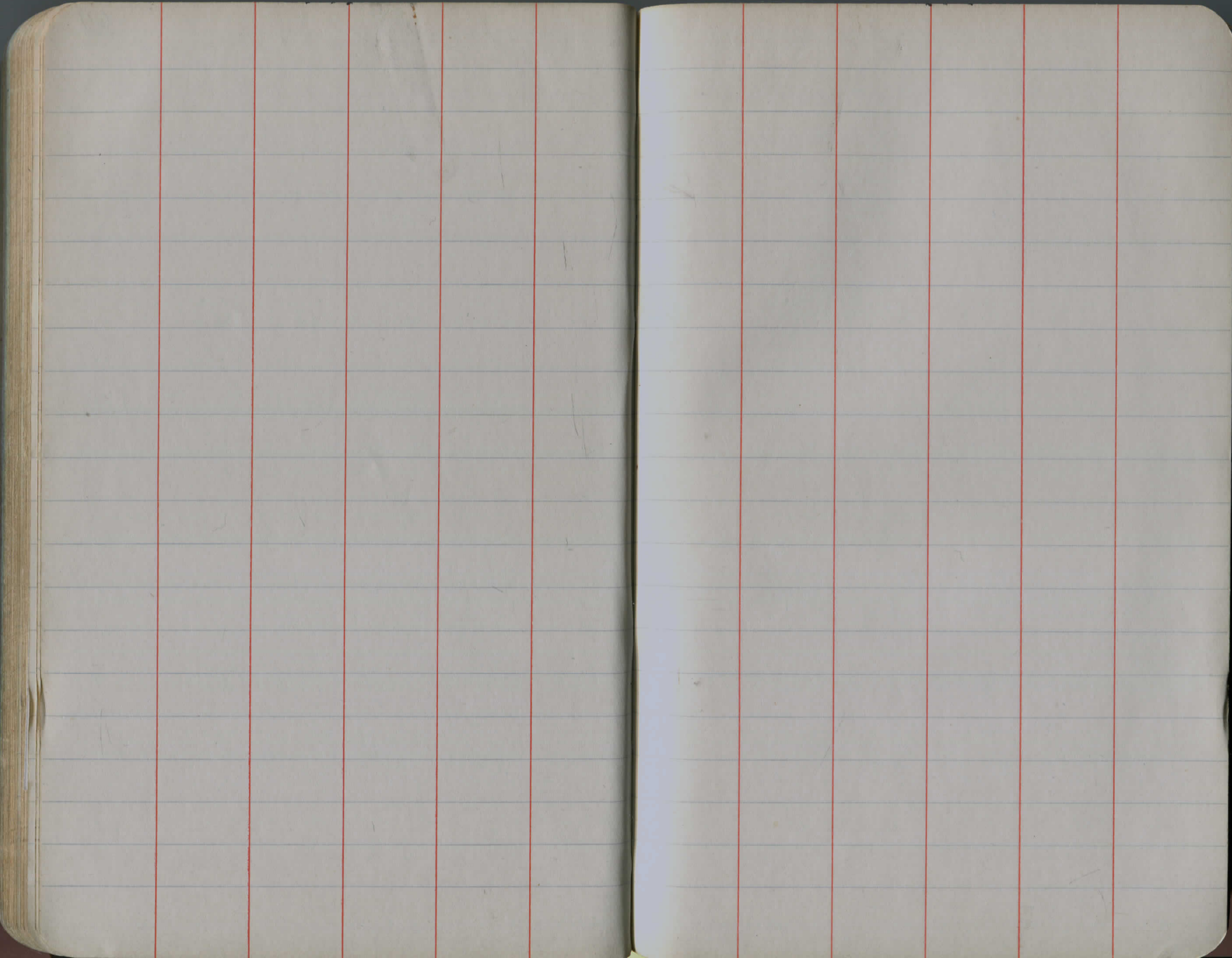


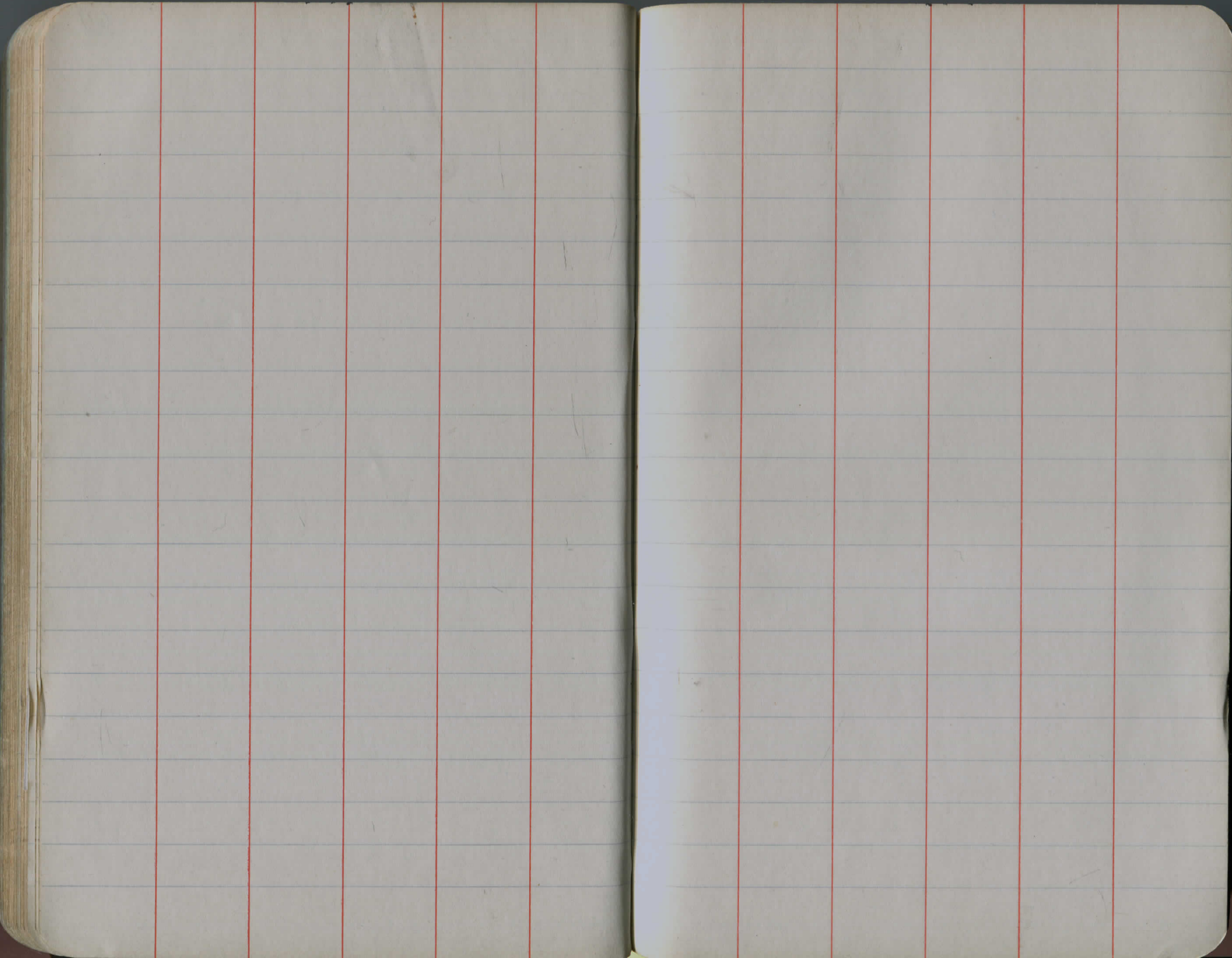


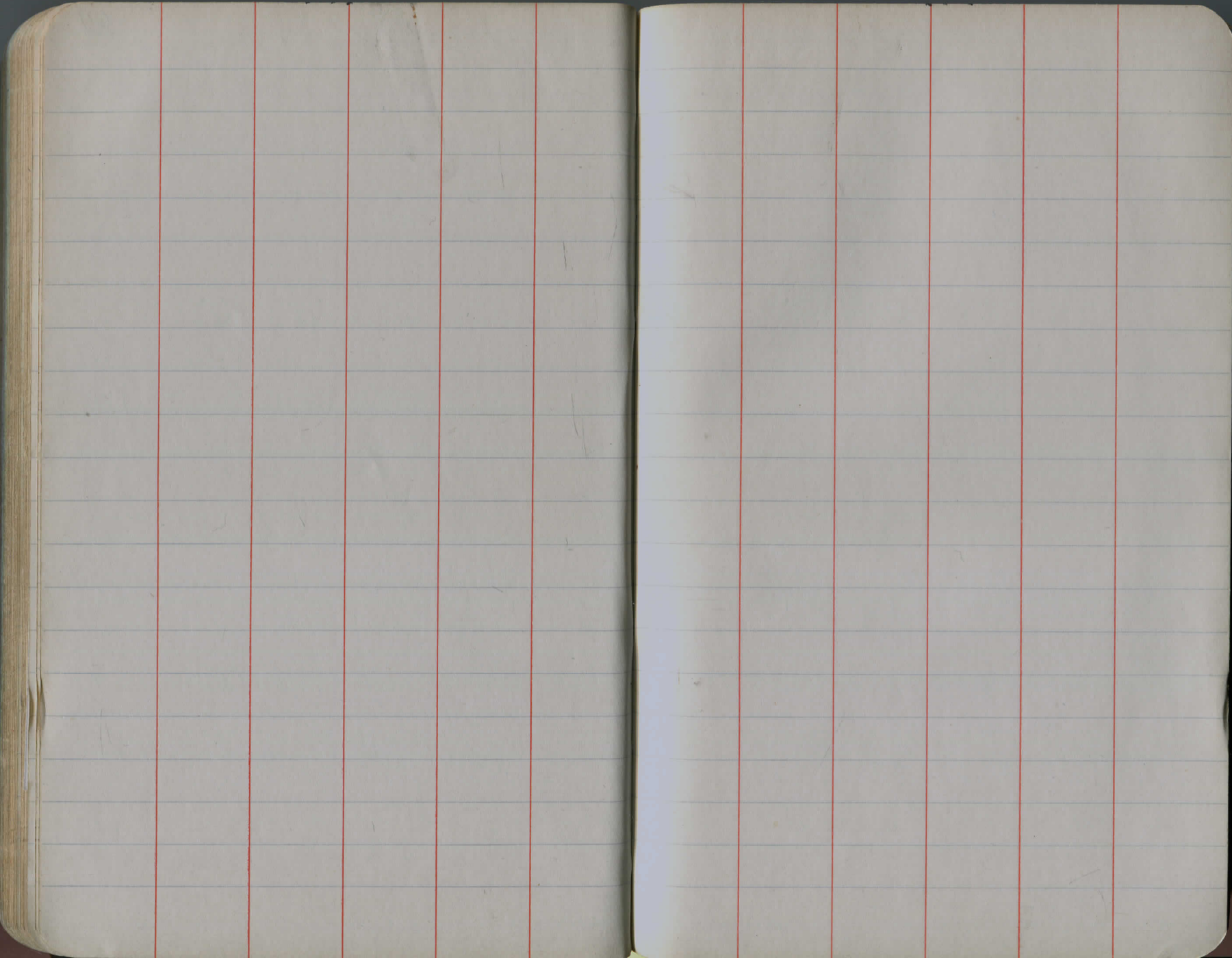




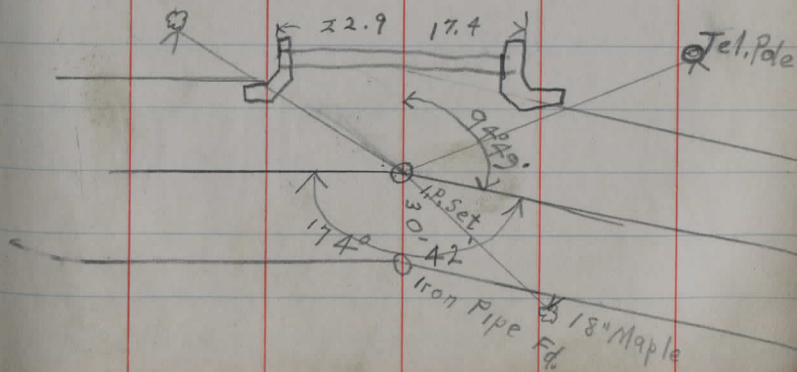




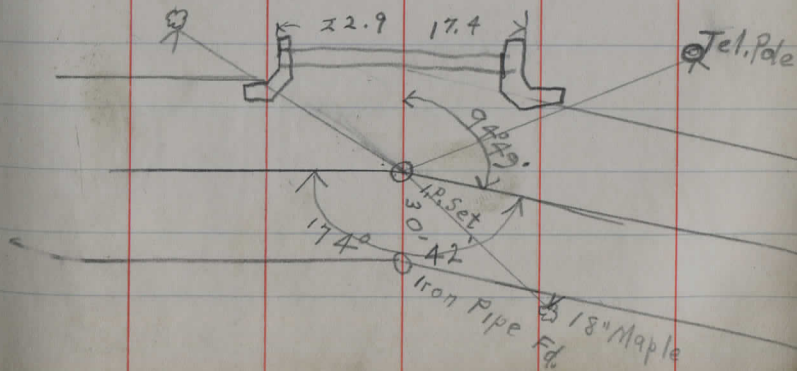




0+19 24" Vit. Pipe Culvert



0+19 24" Vit. Pipe Culvert



thence N (80° or 60°) E, 84 ch. 50 li.
thence N 88° E, 275 ch. 50 li. to the
State Road leading from Chardon
to Ravenna — whole distance
9 miles 7 chains 50 links.

Samuel Penderon, Surveyor,

Book B. P. 480

Vacation of part of above desc. Rd.
-- that part which is west of the
State Road and east of the road
running northerly from Aurora line
by Gen. Eggleston's Mills, ---
a dist. of about 1 mi.

Ordered vacated by Co. Commr.,
Mar. 9, 1831

$$\begin{array}{r} 1.7 \\ 1.8 \\ \hline 2 \\ 6.7 \end{array}$$

6L.6
 96.5

$$\begin{array}{r} 2.00 \\ \hline 2.50 \end{array}$$

$$\begin{array}{r} 5.7 \\ 2.7 \\ \hline 2.5 \\ 1.0 \end{array}$$

$$\begin{array}{r} 3.7 \\ 2.7 \\ \hline 2.6 \end{array}$$

$$\begin{array}{r} 3.00 \\ 3.00 \\ \hline 3.75 \end{array}$$

$$\begin{array}{r} 3.75 \\ 2.50 \\ \hline 1.25 \end{array}$$

1.25

8772 2.9

7 L7

1.25 9.7 10.6/225

Road Records, Book A, P. 244
 Petition, Oct. 30, 1816
 Report, Mar. 2, 1817
 Established, June 3, 1817 as a public high-
 way, agreeable to statute.
 Statute Width, May 1, 1816 to June 1, 1820, 60' or less.
 Survey of a road beginning on the
 West line of the County of Georgia,
 between the lots No 31 + 32, in
 the South Section of Town No. 6
 in the 9th Range, and thence
 running on the line between said
 lots N 88° E 95 chains to the
 Chagrine River, thence N 61° E
 6 ch. 75 ls.,
 thence S. 43° E 4 ch. 7 ls.
 sd. lot line.
 thence N. 88° E. on the same by
 the dwelling house of Gamaliel
 Kent 261 ch. 68 ls.

(Over)

33 2/2
28 5/3
469

506-45
360
146-45

Chas Taylor

July 1 - (2/2) (3/2) (17/2) (29/2)

30.00
11.11
1.00
9.5

12.94

87.06

18+45.77
17+87
58.17

100
28

19+00
18 45.37
54.23

71.47
80.72
7.89

179.60
141.03

28.53

38.57

3/4 24
46

5280 | 11790
10560
12900

49
32

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 12 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR 35 INCH TRACK DIMENSIONMENT.
COURT HOUSE
CHARDON, O.
PHONE 250-X

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 7.0 | 7.2 | 7.3 | 7.5 | 7.6 | 7.8 | 7.9 | 8.1 | 8.2 | 8.4 | 0 |
| 1 | 8.5 | 8.7 | 8.8 | 9.0 | 9.1 | 9.3 | 9.4 | 9.6 | 9.7 | 9.9 | 1 |
| 2 | 10.0 | 10.2 | 10.3 | 10.5 | 10.6 | 10.8 | 10.9 | 11.1 | 11.2 | 11.4 | 2 |
| 3 | 11.5 | 11.7 | 11.8 | 12.0 | 12.1 | 12.3 | 12.4 | 12.6 | 12.7 | 12.9 | 3 |
| 4 | 13.0 | 13.2 | 13.3 | 13.5 | 13.6 | 13.8 | 13.9 | 14.1 | 14.2 | 14.4 | 4 |
| 5 | 14.5 | 14.7 | 14.8 | 15.0 | 15.1 | 15.3 | 15.4 | 15.6 | 15.7 | 15.9 | 5 |
| 6 | 16.0 | 16.2 | 16.3 | 16.5 | 16.6 | 16.8 | 16.9 | 17.1 | 17.2 | 17.4 | 6 |
| 7 | 17.5 | 17.7 | 17.8 | 18.0 | 18.1 | 18.3 | 18.4 | 18.6 | 18.7 | 18.9 | 7 |
| 8 | 19.0 | 19.2 | 19.3 | 19.5 | 19.6 | 19.8 | 19.9 | 20.1 | 20.2 | 20.4 | 8 |
| 9 | 20.5 | 20.7 | 20.8 | 21.0 | 21.1 | 21.3 | 21.4 | 21.6 | 21.7 | 21.9 | 9 |
| 10 | 22.0 | 22.2 | 22.3 | 22.5 | 22.6 | 22.8 | 22.9 | 23.1 | 23.2 | 23.4 | 10 |
| 11 | 23.5 | 23.7 | 23.8 | 24.0 | 24.1 | 24.3 | 24.4 | 24.6 | 24.7 | 24.9 | 11 |
| 12 | 25.0 | 25.2 | 25.3 | 25.5 | 25.6 | 25.8 | 25.9 | 26.1 | 26.2 | 26.4 | 12 |
| 13 | 26.5 | 26.7 | 26.8 | 27.0 | 27.1 | 27.3 | 27.4 | 27.6 | 27.7 | 27.9 | 13 |
| 14 | 28.0 | 28.2 | 28.3 | 28.5 | 28.6 | 28.8 | 28.9 | 29.1 | 29.2 | 29.4 | 14 |
| 15 | 29.5 | 29.7 | 29.8 | 30.0 | 30.1 | 30.3 | 30.4 | 30.6 | 30.7 | 30.9 | 15 |
| 16 | 31.0 | 31.2 | 31.3 | 31.5 | 31.6 | 31.8 | 31.9 | 32.1 | 32.2 | 32.4 | 16 |
| 17 | 32.5 | 32.7 | 32.8 | 33.0 | 33.1 | 33.3 | 33.4 | 33.6 | 33.7 | 33.9 | 17 |
| 18 | 34.0 | 34.2 | 34.3 | 34.5 | 34.6 | 34.8 | 34.9 | 35.1 | 35.2 | 35.4 | 18 |
| 19 | 35.5 | 35.7 | 35.8 | 36.0 | 36.1 | 36.3 | 36.4 | 36.6 | 36.7 | 36.9 | 19 |
| 20 | 37.0 | 37.2 | 37.3 | 37.5 | 37.6 | 37.8 | 37.9 | 38.1 | 38.2 | 38.4 | 20 |
| 21 | 38.5 | 38.7 | 38.8 | 39.0 | 39.1 | 39.3 | 39.4 | 39.6 | 39.7 | 39.9 | 21 |
| 22 | 40.0 | 40.2 | 40.3 | 40.5 | 40.6 | 40.8 | 40.9 | 41.1 | 41.2 | 41.4 | 22 |
| 23 | 41.5 | 41.7 | 41.8 | 42.0 | 42.1 | 42.3 | 42.4 | 42.6 | 42.7 | 42.9 | 23 |
| 24 | 43.0 | 43.2 | 43.3 | 43.5 | 43.6 | 43.8 | 43.9 | 44.1 | 44.2 | 44.4 | 24 |
| 25 | 44.5 | 44.7 | 44.8 | 45.0 | 45.1 | 45.3 | 45.4 | 45.6 | 45.7 | 45.9 | 25 |
| 26 | 46.0 | 46.2 | 46.3 | 46.5 | 46.6 | 46.8 | 46.9 | 47.1 | 47.2 | 47.4 | 26 |
| 27 | 47.5 | 47.7 | 47.8 | 48.0 | 48.1 | 48.3 | 48.4 | 48.6 | 48.7 | 48.9 | 27 |
| 28 | 49.0 | 49.2 | 49.3 | 49.5 | 49.6 | 49.8 | 49.9 | 50.1 | 50.2 | 50.4 | 28 |
| 29 | 50.5 | 50.7 | 50.8 | 51.0 | 51.1 | 51.3 | 51.4 | 51.6 | 51.7 | 51.9 | 29 |
| 30 | 52.0 | 52.2 | 52.3 | 52.5 | 52.6 | 52.8 | 52.9 | 53.1 | 53.2 | 53.4 | 30 |
| 31 | 53.5 | 53.7 | 53.8 | 54.0 | 54.1 | 54.3 | 54.4 | 54.6 | 54.7 | 54.9 | 31 |
| 32 | 55.0 | 55.2 | 55.3 | 55.5 | 55.6 | 55.8 | 55.9 | 56.1 | 56.2 | 56.4 | 32 |
| 33 | 56.5 | 56.7 | 56.8 | 57.0 | 57.1 | 57.3 | 57.4 | 57.6 | 57.7 | 57.9 | 33 |
| 34 | 58.0 | 58.2 | 58.3 | 58.5 | 58.6 | 58.8 | 58.9 | 59.1 | 59.2 | 59.4 | 34 |
| 35 | 59.5 | 59.7 | 59.8 | 60.0 | 60.1 | 60.3 | 60.4 | 60.6 | 60.7 | 60.9 | 35 |
| 36 | 61.0 | 61.2 | 61.3 | 61.5 | 61.6 | 61.8 | 61.9 | 62.1 | 62.2 | 62.4 | 36 |

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.
R.

